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ICI AMERICAS INC VALLEY FORGE PA
DEVELOPMENT OF A 0.01-S DELAY, STAB-INITIATED PRIMER.(U)
DEC 81 J M EVANS

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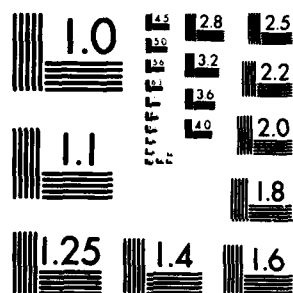
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December 1981

Development of a 0.01-s Delay, Stab-Initiated Primer

John H. Evans

Prepared by

ICI Americas, Inc.
Valley Forge, PA 19482

Under contract

DAAK21-79C-0113

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the design and development testing of a stab initiated delay primer for ordnance application. Its initiation sensitivity is .75 in-oz, delay time is nominally 10 ms, output is 27mg of RD 1333, and its overall size is .16 diameter by .30 long. 650 primers were built and results of shock, temperature, and confinement variable tests on 500 units are presented. Mean function time ranged from about 9 to 12 ms over the temp range of -65F to +160F and the sigma ranged from about 1 to 2 ms. The final design is rugged, reliable, and simple to produce. | | |

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1. INTRODUCTION

Our contract with Harry Diamond Laboratories began in September 1979. It called for the development and pilot lot production of a 0.01-s delay, stab-initiated primer ("stab delay primer") in a package of 0.160-in. diameter by 0.30-in. long. Drawings of this device are shown in appendix A. The primer design is based upon the 0.10-s stab delay primer currently in production for the M734 Multi-Option 60-mm mortar fuze. The assembly drawing of this primer and the assembly drawing of its output cup are shown in appendix B. All other drawings are the same as the 0.01-s device.

2. DEVELOPMENT EFFORT

The original design concept for the 0.01-s primer was to use the same parts that existed for the 0.1-s primer and change the delay powder from boron-barium chromate to zirconium-iron oxide and diatomaceous earth (AlA). Devices were built and tested, but the delay times were too long, being about 0.04-s.

We attempted to reduce this time by decreasing the length of the AlA delay column. Since the length of the output housing is fixed, the length of the lead azide charge had to be increased. Devices were built and tested and many fast function times (instants) resulted.

We felt these instants were caused by having the lead azide too close to the input charge. Primers were built and tested with a spacer in the output assembly which moved the lead azide back to its original position and kept the short AlA column required for the proper time. With this design many duds resulted.

If the delay powder was too far from the input charge, duds resulted; if the lead azide was too close to the input charge, instants resulted. We decided to replace the output cup with a heavy-walled machined part. This would give better mechanical support to the lead azide and allow closer placement of it to the input charge to eliminate the dud problem. Stainless-steel output cups were tried, but many instants resulted. We then switched to aluminum cups and test results were significantly improved. The dud and instant problems were still present, but we found that these could be eliminated by increasing the cup bottom thickness and controlling the air gap between the input charge and the top of the delay column.

The cup as shown in appendix A gave good support, yet the bottom was easily blown out by the lead azide charge. If the air gap was greater than 0.06-in., duds resulted; if it was less than 0.02-in., instants resulted. The gap is controlled at 0.03 to 0.045-in.

The final design is shown in appendix A. The Housing, Input Cup Assembly, and Baffle Screen are the same parts as are in the 0.1-s design. The Output Cup Assembly is not the same. It consists of a machined aluminum cup which contains the lead azide output charge and the AlA delay column. The lead azide charge is 27 mg versus 17 mg for the 0.1-s design.

This increase was necessary to meet the delay column height requirements for the 0.01-s delay time and also to meet the air gap requirements. The ALA charge is 9 mg.

2.1 Preproduction of Primer

A total of 137 primers were built to the design of appendix A and tested using the test fixture shown in appendix C. The tests were conducted at +150°F, 70°F, and -65°F. The detailed test results are shown in appendix D and a summary is shown in table 1.

The first group of 25 primers had slow times and the ALA charge weight was reduced to 9 mg from 11 mg for the balance of the devices. All times except one were within specification (0.005 to 0.015-s) and there were no duds or instants.

TABLE 1. SUMMARY: PREPRODUCTION TESTS

| Test condition (°F) | Quantity | Mean (m-s) | Standard deviation (m-s) |
|------------------------|----------|---------------|-----------------------------|
| 70 | 25 | 12.32 | 1.62 |
| 70 | 10 | 10.82 | 1.67 |
| -65 | 40 | 11.99 | 1.89 |
| 150 | 40 | 11.19 | 1.59 |
| 70 | 22 | 11.51 | 1.18 |

2.2 Pilot Lot Primers

A total of 500 primers were built to the drawings of appendix A for the pilot lot. One hundred and fifty of these were selected for testing. Fifty were functioned at +150°F, 50 were functioned at -65°F, and 50 were functioned at 70°F. The 70°F units were functioned after being subjected to the following shock pulses (required by the specifications):

The primer will be subjected to two (2) consecutive triangular shock pulses, each of 10,000 \pm 2000 g peak amplitude and approximately 1.0 millisecond total pulse width. The two (2) pulses will be applied axially. The acceleration vector of the first pulse will be directed from the stab end of the primer toward its output end. The acceleration vector of the second pulse will be in the reverse direction.

The primer will be subjected to the same shock test as above but at a peak amplitude pulse level of 40,000 g max.

The test samples were inspected and tested in accordance with the ICI procedure shown in appendix E. The testing was performed at the ICI plant in Tamaqua, PA, and the test fixture was essentially the same as is shown in appendix C. With the Tamaqua fixture, the drop weight is allowed to exit from the guide tube before it contacts the firing pin. At the Valley Forge plant, the drop weight did not exit from the guide tube before contacting the firing pin. The significance of this difference will be discussed in section 2.3.

The detailed test results are shown in appendix F and summarized in table 2. The results were not within specification, the times were long, and a total of 9 duds resulted. We assumed that a design flaw existed and began to consider new design approaches.

TABLE 2. SUMMARY: PILOT LOT TESTS

| Test condition (°F) | Quantity | Mean (m-s) | Standard deviation (m-s) |
|------------------------|-------------|---------------|-----------------------------|
| 70* | 50 (4 duds) | 14.44 | 2.97 |
| 65 | 50 (3 duds) | 15.09 | 3.18 |
| 150 | 50 (2 duds) | 14.20 | 2.62 |

*25 were subjected to a 10,000-g triangular shock pulse.
25 were subjected to a 40,000-g triangular shock pulse.

2.3 Continued Development

Many new design approaches were considered and those that appeared to be the most promising were built and tested.

Four groups of primers were built with varying charge weight and density of the output charge of the input cup assembly. In all groups but one, duds resulted, and long delay times resulted in the group with no duds. As a result it was decided to remain with the standard input cup assembly.

Other tests were run where a flash charge of $Ti/KClO_4$ was added on top of the delay column. This charge was not pressed, but lightly consolidated with the insertion of the input cup assembly. This charge was added to provide easier ignition of the delay column and to help cushion the output shock of the input primer assembly. We had initial success but additional testing exhibited a severe instant problem.

At this point we decided to investigate the test method and discovered the difference in the test methods versus test location as

mentioned in the Pilot Lot section (2.2) of the report. Given this difference, we decided that the Valley Forge test method would confine the primer more and thus prevent the output of the input charge from exiting out the top of the primer. This would force the flame at the delay column and thus provide better ignition.

2.4 Survey Tests

An additional 50 primers were selected at random from the Pilot Lot. These were tested at Valley Forge with the Valley Forge fixture and test procedure. All tests were at 70°F and no duds, or instants resulted. The times were much more like the preproduction tests rather than the pilot lot tests. In addition, three other tests of varying degrees of confinement were run with small samples from the pilot lot primers. The detailed test results are shown in appendix G and summarized in table 3. These tests did show that the delay times were a function of test method.

TABLE 3. SUMMARY: SURVEY TEST RESULTS

| Test condition (°F) | Quantity | Mean (m-s) | Standard deviation (m-s) |
|-----------------------------------|----------|---------------|-----------------------------|
| 70 (samples from pilot lot) | 50 | 12.40 | 1.74 |
| 70 ¹ | 10 | 10.25 | 1.03 |
| 70 ² | 5 | 8.45 | 1.39 |
| 70 ³ | 5 | 12.31 | 2.30 |

¹Highly confined--firing pin weight remained in guide tube.

²Little confinement--firing pin weight exists from guide tube.

³Little confinement--to simulate the Tamaqua test method.

2.5 Confinement Test Program

As a result of the survey tests, it was decided to select an additional 130 primers for a confinement test program.

2.5.1 Test Program

The 130 primers were divided into seven test groups and a group of five spares. These groups were designed to investigate the effects of confinement, firing pin penetration, test fixture type, and temperature. The test groups are described as follows:

(a) 15 units at -65°F in HDL test fixture designed to simulate the SHAWL fuze.

(b) 15 units at 70°F in same test fixture.

(c) 15 units at 160°F in same test fixture.

(d) 20 units at 70°F in ICI drop test fixture with maximum input confinement and firing pin penetration controlled to 0.02-in.

(e) 20 units at 70°F in ICI drop test fixture with minimum input confinement and firing pin penetration controlled to 0.02-in.

(f) 20 units at 70°F in ICI drop test fixture with maximum input confinement and firing pin penetration controlled to 0.06-in.

(g) 20 units at 70°F in ICI drop test fixture with minimum input confinement and firing pin penetration controlled to 0.06-in.

2.5.2 Test Fixtures

A drawing of the HDL fixture is shown in appendix H. In this fixture, a 6.6-lb weight is dropped on a firing pin, shearing a safety wire, and driving the pin into the primer. The firing pin point diameter was 0.015-in. and the depth of penetration was 0.04-in. The heavy drop-weight represents 1300 times the weight of the normal fuze firing pin. Although this is only 5 to 20% of the force created by deceleration of the firing pin at target impact, it did provide a much higher degree of input confinement than normally encountered in laboratory tests.

The ICI fixture is shown in appendix I (drawing D-8291). A 337-gram weight was dropped on a conventional 0.03-diam firing needle having a 26°, 0.005-diam flat point. The needle is guided by a steel cover over the primer. This cover has provision for a replaceable plastic guide sleeve that can be placed over the primer to confine back-blast from its initiation. The firing needle passed through a close-fitting hole in the block. The block is omitted for the "unconfined" tests. Firing pin penetration is controlled by a precision machined shoulder pin used to drive the firing needle. It would shoulder-out on the steel guide-block after the correct penetration. The details of each test set-up are shown as sections A, B, C, and D of drawing D-8291 (appendix I).

2.5.3 Instrumentation

Instrumentation for the time measurements was by means of a piezoelectric accelerometer rigidly attached to the metal test fixture structure. Output of the accelerometer was monitored directly by a dig-

ital storage oscilloscope. The "sound" produced by the primer's input and output charges functioning could be "heard/seen" on the scope trace, and the function time was determined with a resolution of 50 μ s.

2.5.4 Test Results

The test data sheets and statistical calculations for the 125 primers are shown in appendix J. A summary of the test results is shown in figure 1. This figure contains the mean function time and standard deviation for each test group and a histogram for each group all aligned to the same time scale.

2.5.5 Discussion

Results for the ICI fixture show that confinement made a difference for the 0.02 firing pin penetration, with high confinement giving shorter function times by roughly 15%. When firing pin penetration was increased to 0.06, there was no apparent difference in function time due to differences in confinement. The average times for both confinements were in between those obtained for the 0.02 penetration case.

Results with the fuze fixture show the expected dependence on temperatures; hot--fast, cold--slow. The ambient results most closely match the unconfined cases with the ICI fixtures. This may be due to the fact that a pressure of only 150 PSI is needed on the wide face of the fuze firing pin in order to lift the heavy drop weight. Pressure created by the input charge function is expected to be much greater than this so the firing pin probably moved back and considerably relieved the confining pressure before the 10-ms delay was completely burned.

Although the results obtained in these tests show that the degree of primer input confinement and firing pin penetration obtained in an actual fuze configuration can make a difference in performance, they do not entirely explain the large differences in results obtained in preliminary testing with different fixtures. Some of these differences must be attributed to unresolved differences in instrumentation or test technique, or perhaps to the usual inconsistency of small sample statistics.

With HDL test fixture, two failures occurred (failure to initiate the input mix). One primer was replaced (-65°F) and the second was not ($+165^{\circ}\text{F}$). The failures were attributed to the heavy shear wire used in the test fixture which considerably reduced the velocity of the drop weight. This result would be expected when the NOL 130 input explosive mix is punctured at a very low velocity. No such input duds occurred in over 450 tests that have been run on the same primers when using a higher velocity impact in a different fixture.

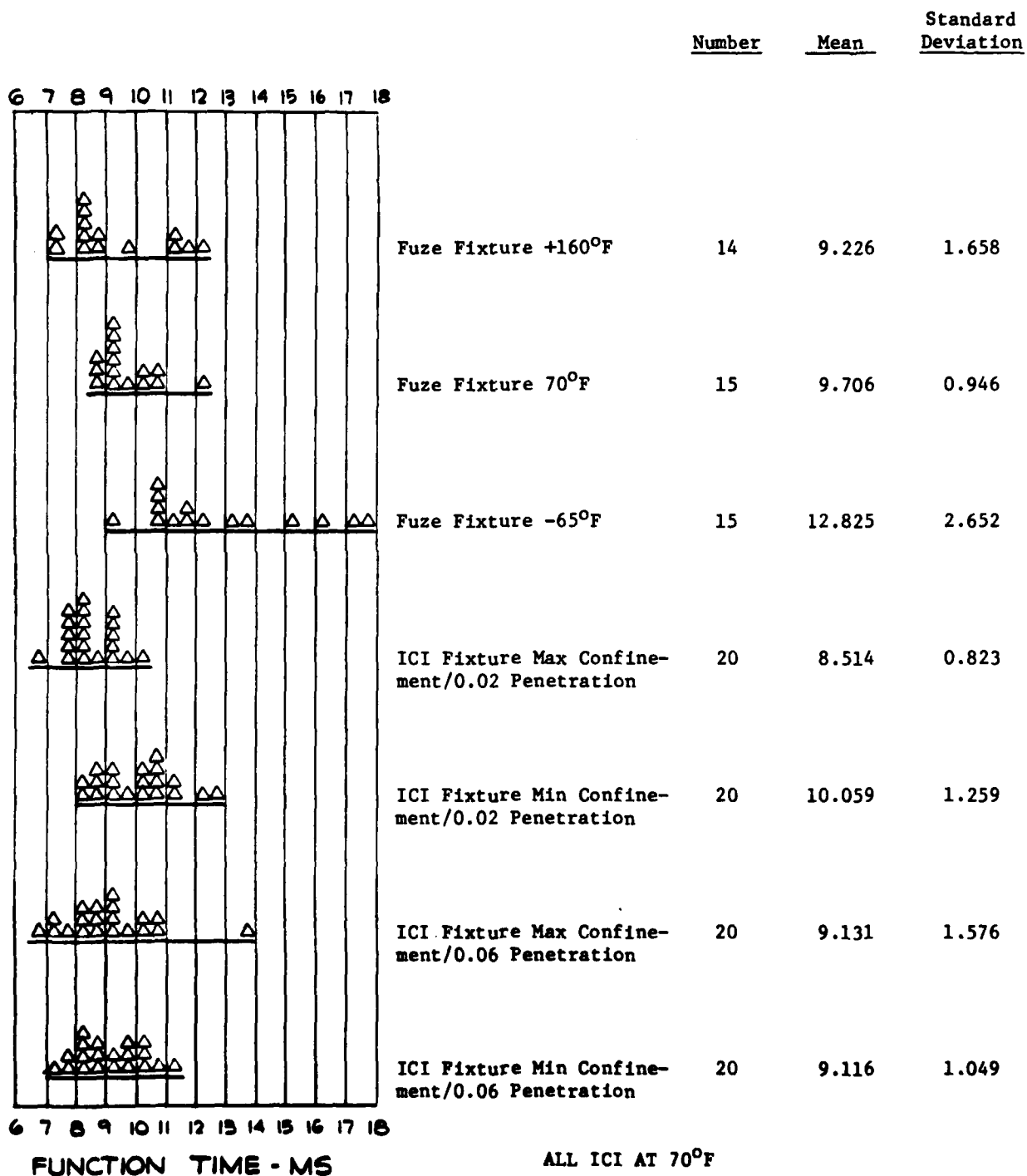


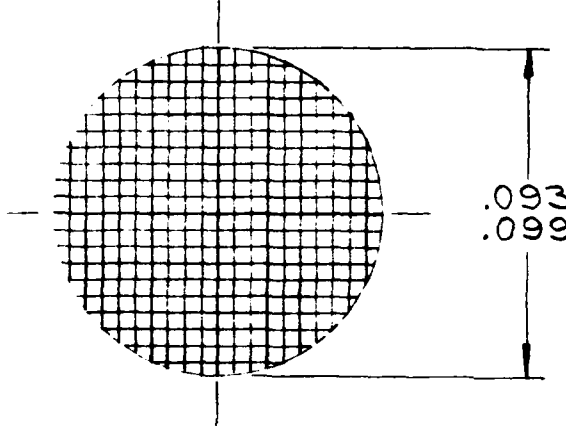
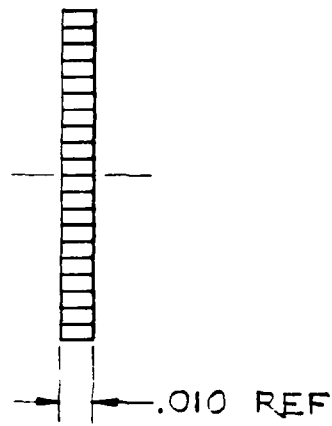



FIGURE 1. SUMMARY OF CONFINEMENT TESTS

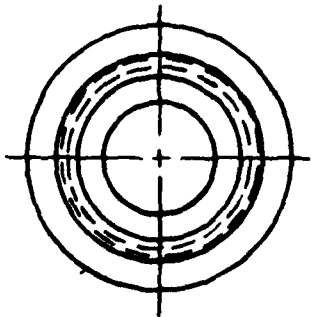
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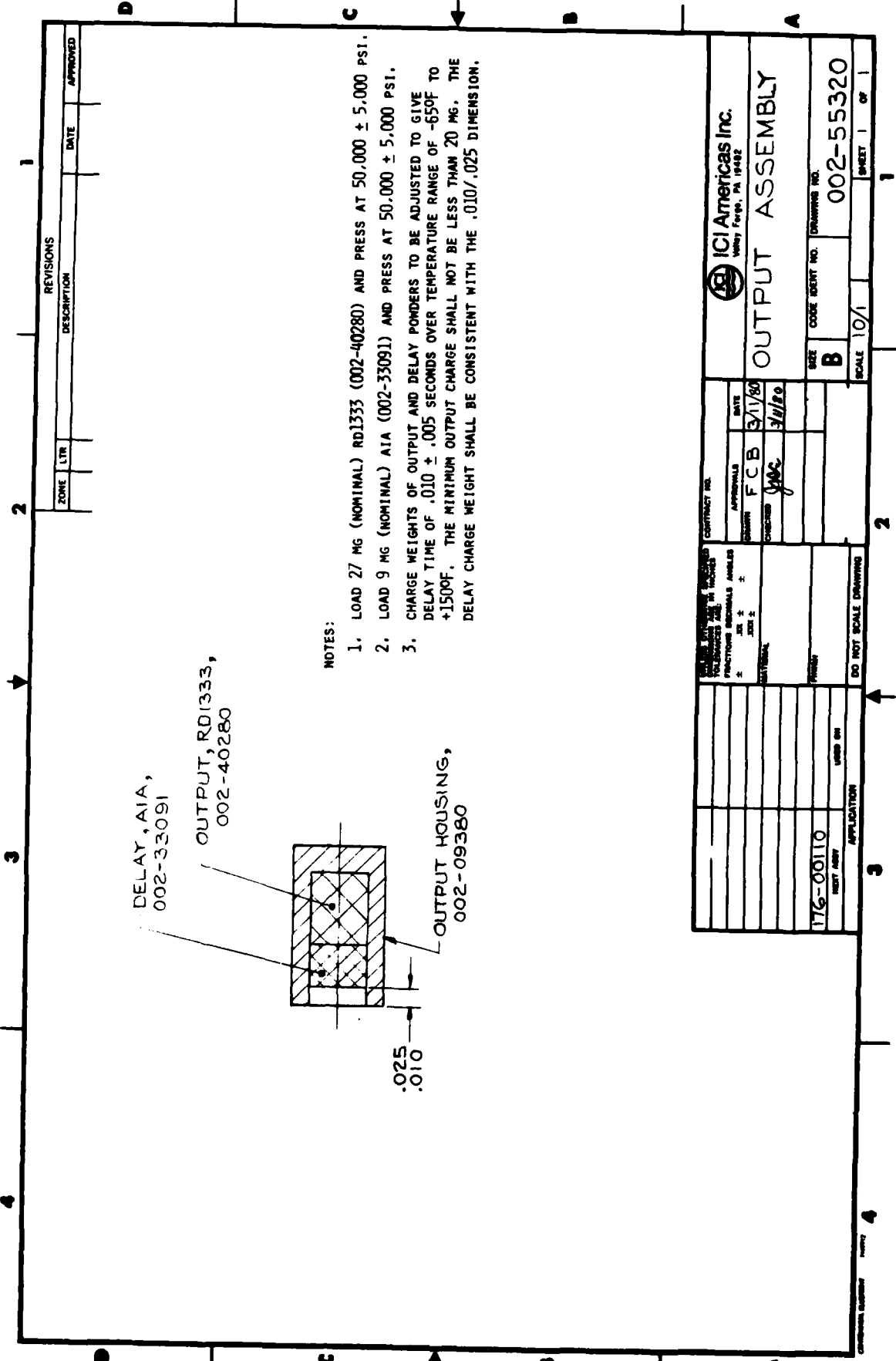
APPENDIX A.--0.01-S STAB DELAY PRIMER DRAWINGS

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| <div style="display: flex; justify-content: space-around; align-items: center;">   </div> | | | | | | | | | |
| NOTES: 1. PARTS SHALL BE DIE CUT & FREE OF EXCESSIVE RAGGED EDGES, BURRS, & SLIVERS. | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%; vertical-align: top;"> MAT'L: 100 MESH STAINLESS STEEL, .010THK </td> <td style="width: 30%; vertical-align: top;"> SCALE: 20/1 DRAWN BY: FCB CHECKER: PROJECT ENG: WELKER APPROVED BY: DATE: 3-6-75 </td> <td style="width: 40%; vertical-align: top; text-align: center;"> BAFFLE SCREEN  ATLAS AEROSPACE DIVISION ICI United States Inc. Valley Forge, PA 19082 </td> </tr> <tr> <td style="vertical-align: top;"> TOLERANCES .XX± ~ .XXX± ~ ANGLES ± ~ FINISH IS IN ENGRINGERS </td> <td style="vertical-align: top;"> 176-00060 NEXT ASSY. </td> <td style="vertical-align: bottom;"> SHEET 1 OF 1 </td> </tr> </table> | | | | MAT'L: 100 MESH STAINLESS STEEL, .010THK | SCALE: 20/1 DRAWN BY: FCB CHECKER: PROJECT ENG: WELKER APPROVED BY: DATE: 3-6-75 | BAFFLE SCREEN  ATLAS AEROSPACE DIVISION ICI United States Inc. Valley Forge, PA 19082 | TOLERANCES .XX± ~ .XXX± ~ ANGLES ± ~ FINISH IS IN ENGRINGERS | 176-00060 NEXT ASSY. | SHEET 1 OF 1 |
| MAT'L: 100 MESH STAINLESS STEEL, .010THK | SCALE: 20/1 DRAWN BY: FCB CHECKER: PROJECT ENG: WELKER APPROVED BY: DATE: 3-6-75 | BAFFLE SCREEN  ATLAS AEROSPACE DIVISION ICI United States Inc. Valley Forge, PA 19082 | | | | | | | |
| TOLERANCES .XX± ~ .XXX± ~ ANGLES ± ~ FINISH IS IN ENGRINGERS | 176-00060 NEXT ASSY. | SHEET 1 OF 1 | | | | | | | |
| NO. 002-29300 | | | | | | | | | |



| PART NO. | " C " | " D " | " E " | USED ON |
|-----------|-------------|---|----------|---------|
| 002-08770 | .020 ± .002 | .215 ^{+ .005} _{-.000} | .318 MAX | SDP |
| 002-08771 | .035 ± .002 | .238 ^{+ .005} _{-.000} | .356 MAX | SDD |

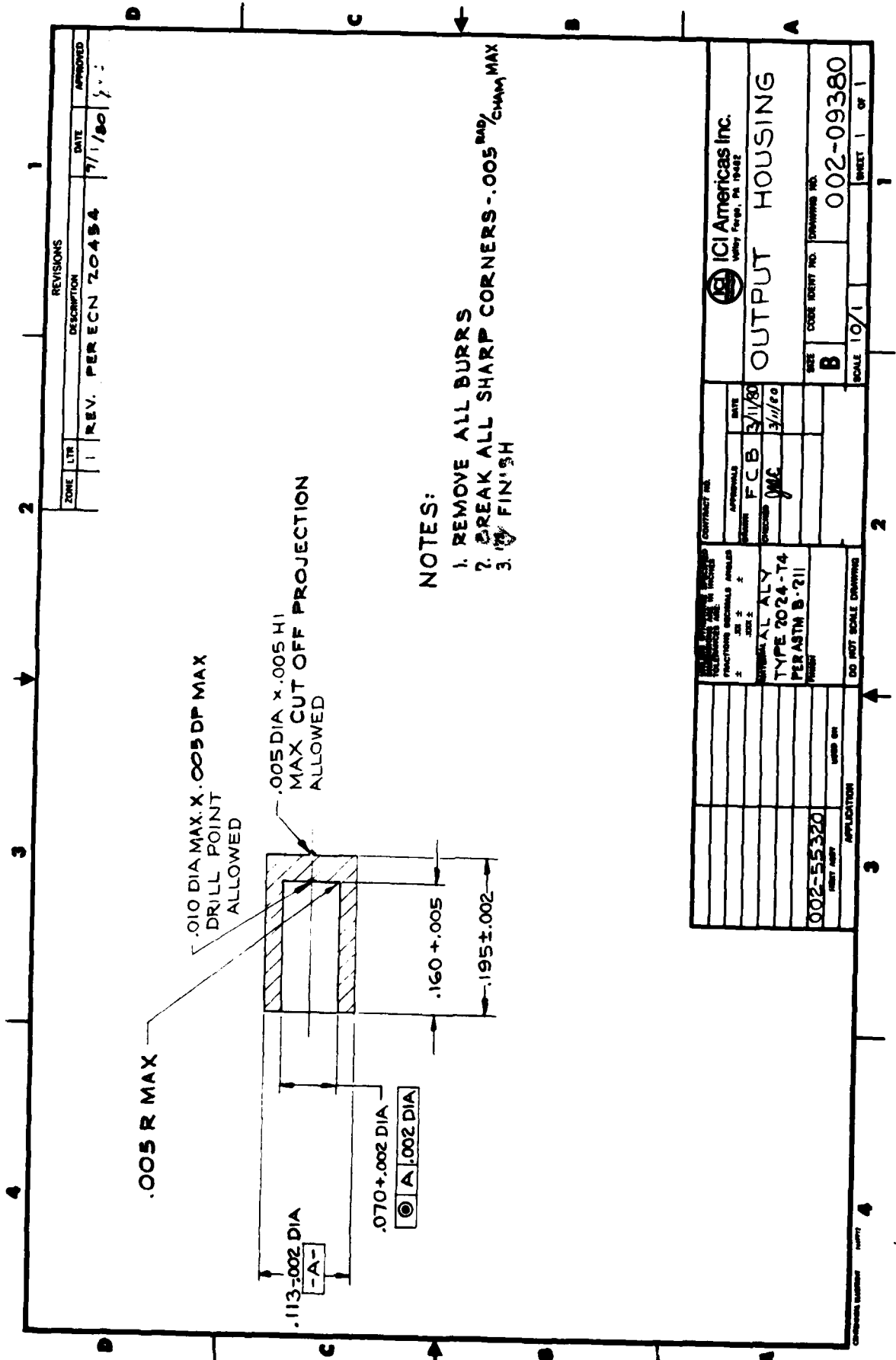
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NOTES:

1. LOAD 27 MG (NOMINAL) RD1333 (002-40280) AND PRESS AT 50,000 \pm 5,000 PSI.
2. LOAD 9 MG (NOMINAL) AIA (002-33091) AND PRESS AT 50,000 \pm 5,000 PSI.
3. CHARGE WEIGHTS OF OUTPUT AND DELAY POWDERS TO BE ADJUSTED TO GIVE DELAY TIME OF .010 \pm .005 SECONDS OVER TEMPERATURE RANGE OF -65OF TO +150OF. THE MINIMUM OUTPUT CHARGE SHALL NOT BE LESS THAN 20 MG. THE DELAY CHARGE WEIGHT SHALL BE CONSISTENT WITH THE .010/.025 DIMENSION.

| | | | |
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| ICI Americas Inc. Valley Forge, PA 19482 | | CONTRACT NO. 176-00110 | |
| APPROVALS FCB 3/1/80 JWC 3/1/80 | DATE 3/1/80 | DRAWING NO. 002-55320 | |
| OUTPUT ASSEMBLY | | SIZE B | SCALE 10/1 |
| DO NOT SCALE DRAWING | | SHEET 1 OF 1 | |



- NOTES:
1. REMOVE ALL BURRS
 2. BREAK ALL SHARP CORNERS-.005 ^{RAD} CHAM MAX
 3. ^{1/4} FINISH

| REVISIONS | | |
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| ZONE | LTR | DESCRIPTION |
| 1 | 1 | REV. PER ECN 70454 |
| | | DATE 7/1/80 |
| | | APPROVED |

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|--|--------------------------|
| ICI Americas Inc. Valley Forge, PA 19482 | |
| OUTPUT HOUSING | |
| SIZE CODE B | DRAWING NO. 002-09380 |
| SCALE 10/1 | SHEET 1 OF 1 |
| CONTRACT NO. | DATE 3/1/80 |
| APPROVALS | DESIGNED JMC |
| CHECKED | DATE 3/1/80 |
| MATERIAL ALY TYPE 2024-T4 PER ASTM B-211 | DO NOT SCALE DRAWING |
| PART NO. 002-55320 | APPLICATION |

| NO. | REVISIONS | DATE |
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| 3. | REDRAWN WITH P/M 002-33091 ADDED ECN 10564 | 4/16/70 JLH |

IGNITION COMP. A-1A

PER MIL-P-22264

| PART NO. | TYPE | 000-00750 ZIRCONIUM POWDER | 000-15250 IRON OXIDE (FERRIC OXIDE) | 002-33430 DIATOMACEOUS EARTH |
|------------|--------------------------|----------------------------------|---|------------------------------------|
| 002-33090* | STANDARD | | | |
| 002-33091 | MODIFIED (SEE NOTE 3) | 64.25% | 24.25% | 11.50% |

NOTES:

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3. PERCENTAGES BY WEIGHT PER MIL-P-22264 DO NOT APPLY.

TYPE OF CERTIFICATION


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QUANTITATIVE ☒ _____

NONE _____

*DESIGN PREPARED FOR LMSC/MSD AND
GOVERNMENT PRIME CONTRACT UNDER
GOVERNMENT PRIME NO. NO 003066C0186.

PROPRIETARY INFORMATION OF
ATLAS CHEMICAL INDUSTRIES, INC.

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| MAT'L: _____ UNLESS OTHERWISE NOTED DIMENSIONS ARE IN INCHES FRACTIONS $\frac{\Delta}{\Delta}$ ANGLES Δ DECIMALS Δ FINISH IS IN MICROINCHES | | SCALE _____ DRAWN BY _____ CHECKER _____ PROJECT ENG. _____ APPROVED BY _____ APPROVED BY _____ DATE _____ | IGNITION COMP. A-1A  ATLAS CHEMICAL INDUSTRIES, INC. WILMINGTON 98, DEL. AEROSPACE COMPONENTS DIVISION |
| 002-33430 250-02210 NEXT ASST. _____ | | SHEET 1 OF 1 | NO. 002-33090 |

| APPLICATION | | REVISION | | | |
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| | | 2 | Correct Sources. ECN 14847 | 8/9/79 | PfR |

ARCON 2795 (003-87190) 70%

VERSAMID 125 (003-87180) 30%

APPROVED SOURCE:

ARCON 2795 - ALLIED RESIN CORP.
EAST WEYMOUTH, MASS. 02189

VERSAMID 125 - GENERAL MILLS
CHEMICAL DIV.
KANKAKEE, ILL.

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SCALE

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REVISIONS

DATE

VERSAMID 125
(NYLON RESIN)

QUALITATIVE - CERT.
SUGG. SUPPLIER - GENERAL MILLS
CHEMICAL DIV.
KANKAKEE, ILL.

MAT'L:

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DIMENSIONS ARE IN INCHES

FRACTIONS Δ ANGLES Δ DECIMALS Δ

FINISH IS IN MICRONS

SCALE

DRAWN BY

CHECKER

PROJECT ENG.

APPROVED BY

APPROVED BY

DATE

NEXT ASST.

VERSAMID 125



ATLAS CHEMICAL INDUSTRIES, INC.

WILMINGTON 98, DEL.

AEROSPACE COMPONENTS DIVISION


SHEET OF

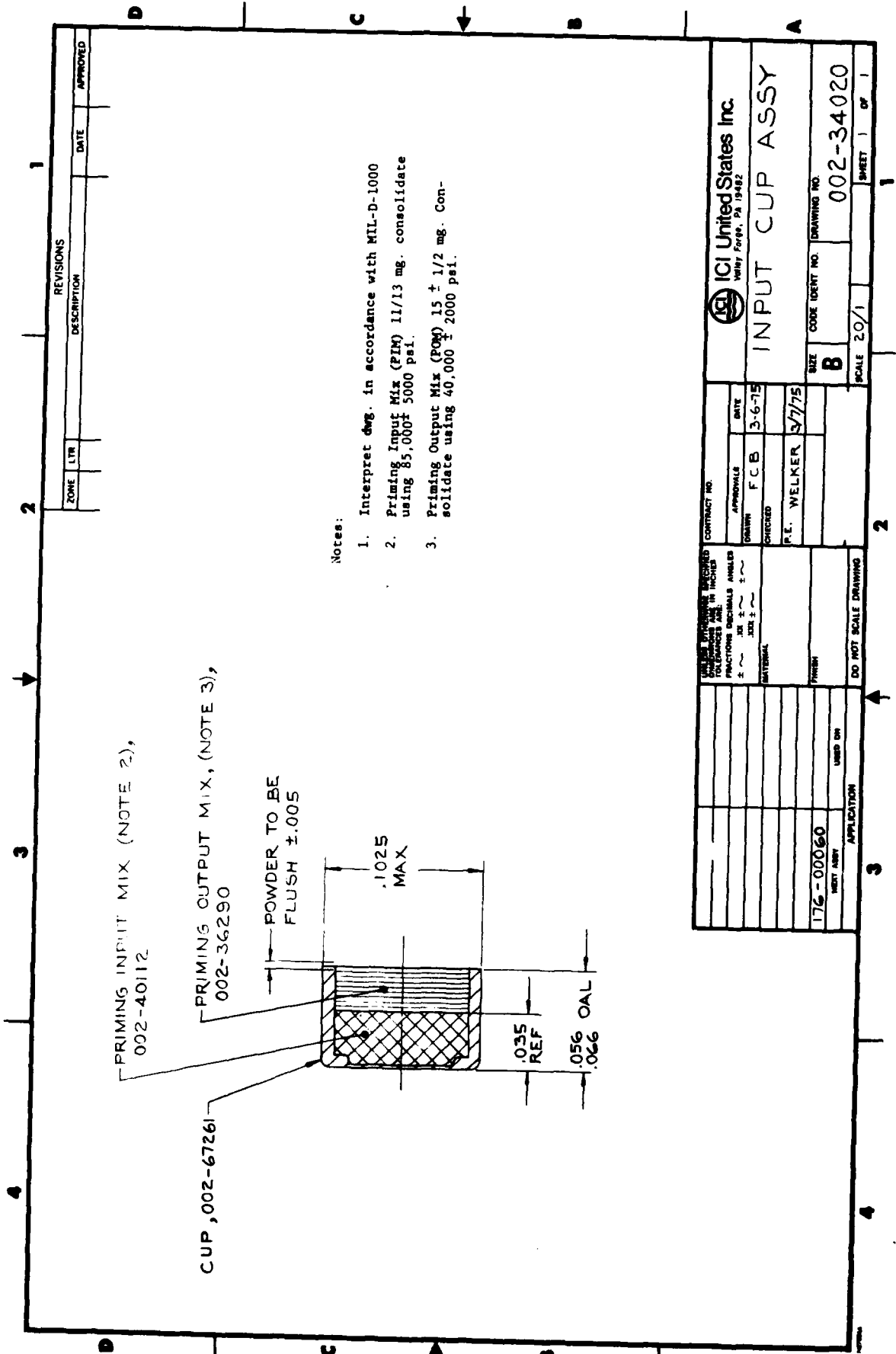
NO. 003-87180

| NO. | REVISIONS | DATE |
|-----|-----------------------------------|---------|
| 1 | WAS ERL 2795 ECN 16405 <i>ADD</i> | 3/24/75 |

ARCON 2795
(EPOXY RESIN)

QUALITATIVE CERT.
SUGG. SUPPLIER - ALLIED RESIN CORP.
EAST WEYMOUTH, MASS. 02189

| | | | |
|---|-------------------|--------------------|---|
| MAT'L: UNLESS OTHERWISE NOTED DIMENSIONS ARE IN INCHES FRACTIONS ▴ ANGLES ▴ DECIMALS ▴ FINISH IS IN MICROINCHES | | SCALE _____ | ARCON 2795  ATLAS CHEMICAL INDUSTRIES, INC. WILMINGTON 99, DEL. AEROSPACE COMPONENTS DIVISION |
| | | DRAWN BY _____ | |
| | | CHECKER _____ | |
| | | PROJECT ENG. _____ | |
| | | APPROVED BY _____ | |
| | APPROVED BY _____ | | |
| | NEXT ASSY. | DATE _____ | SHEET OF NO. 003-87190 |



- Notes:
1. Interpret dwg. in accordance with MIL-D-1000
 2. Priming Input Mix (PIM) 11/13 mg. consolidate using 85,000 ± 5000 psi.
 3. Priming Output Mix (POM) 15 ± 1/2 mg. Con-solodate using 40,000 ± 2000 psi.

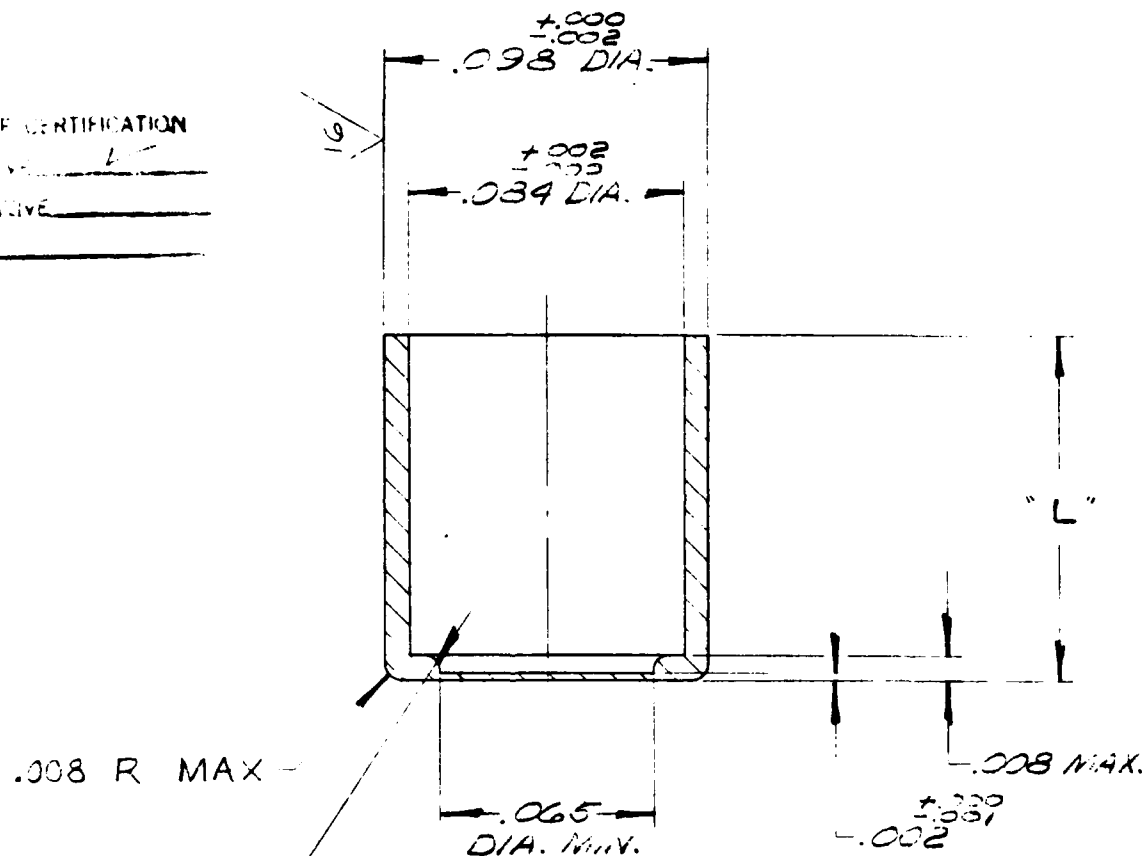
| | | | |
|---|---------------------|--------------------------|------------|
| ICI United States Inc. Valley Forge, Pa 19402 | | INPUT CUP ASSY | |
| CONTRACT NO. APPROVALS DRAWN FCB CHECKED P.E. WELKER DATE 3-6-75 | CODE IDENT NO. B | DRAWING NO. 002-34020 | SCALE 20/1 |
| USE THIS DRAWING FOR THE FOLLOWING PARTS: 1. 172-00060 2. 172-00060 3. 172-00060 4. 172-00060 5. 172-00060 6. 172-00060 7. 172-00060 8. 172-00060 9. 172-00060 10. 172-00060 11. 172-00060 12. 172-00060 13. 172-00060 14. 172-00060 15. 172-00060 16. 172-00060 17. 172-00060 18. 172-00060 19. 172-00060 20. 172-00060 21. 172-00060 22. 172-00060 23. 172-00060 24. 172-00060 25. 172-00060 26. 172-00060 27. 172-00060 28. 172-00060 29. 172-00060 30. 172-00060 31. 172-00060 32. 172-00060 33. 172-00060 34. 172-00060 35. 172-00060 36. 172-00060 37. 172-00060 38. 172-00060 39. 172-00060 40. 172-00060 41. 172-00060 42. 172-00060 43. 172-00060 44. 172-00060 45. 172-00060 46. 172-00060 47. 172-00060 48. 172-00060 49. 172-00060 50. 172-00060 51. 172-00060 52. 172-00060 53. 172-00060 54. 172-00060 55. 172-00060 56. 172-00060 57. 172-00060 58. 172-00060 59. 172-00060 60. 172-00060 61. 172-00060 62. 172-00060 63. 172-00060 64. 172-00060 65. 172-00060 66. 172-00060 67. 172-00060 68. 172-00060 69. 172-00060 70. 172-00060 71. 172-00060 72. 172-00060 73. 172-00060 74. 172-00060 75. 172-00060 76. 172-00060 77. 172-00060 78. 172-00060 79. 172-00060 80. 172-00060 81. 172-00060 82. 172-00060 83. 172-00060 84. 172-00060 85. 172-00060 86. 172-00060 87. 172-00060 88. 172-00060 89. 172-00060 90. 172-00060 91. 172-00060 92. 172-00060 93. 172-00060 94. 172-00060 95. 172-00060 96. 172-00060 97. 172-00060 98. 172-00060 99. 172-00060 100. 172-00060 | | DO NOT SCALE DRAWING | |

| PART NO. | "L" | NO. | REVISIONS | DATE |
|-----------|-------------------------------|-----|---|-----------------------|
| 002-67260 | .105 $\pm .000$ $\pm .005$ | 1. | ADD P/N-67261, FINISH & TAB LENGTH ECN 16299 | 10-9-74 <i>RSE</i> |
| 002-67261 | .065 $\pm .005$ $\pm .000$ | 2. | REV PER ECN 16338 <i>RDU</i> | 11-11-74 |
| | | 3. | .065 WAS $\pm .000$ $\pm .005$ $\pm .008$ R WAS $\pm .005$ $\pm .010$ ECN 16783 <i>RDU</i> | 11-25-76 |


TYPE OF CERTIFICATION

QUANTITATIVE

NONE



- NOTES
1. SPEC MIL-A-2550 APPLIES.
 2. MATERIAL: ALUMINUM 7075-T6, 1/8" D, SHAFT CH 375 P, 375 P, 457 P, 500 P
 3. $\sqrt{}$ ALL OVER EXCEPT AS NOTED.

| | | | |
|--|------------|--|--------------|
| MAT'L: | | SCALE 20:1 | |
| | | DRAWN BY <i>RW</i> | |
| UNLESS OTHERWISE NOTED DIMENSIONS ARE IN INCHES | | CHECKER | |
| FRACTIONS $\frac{1}{2}$ ANGLES 45° | | PROJECT ENG <i>Bu</i> | |
| DECIMALS $\frac{1}{10}$ | | APPROVED BY | |
| FINISH IS IN MICRONS | | APPROVED BY | |
| | NEXT ASST. | DATE 7-2-69 | SHEET 1 OF 1 |
| | |  ATLAS AEROSPACE DIVISION ICI United States Inc. Valley Forge, PA 19482 | |
| | | NO. 002-67261 | |

PRIMER OUTPUT MIXTURE


NOTE 2

| COMPOSITION BY WEIGHT | MATERIAL | ICI PN | SPECIFICATION | SIEVE SIZE NOTE 1 |
|--------------------------|--------------------|-----------|---------------|----------------------|
| 11 ± 1.0% | LEAD AZIDE, RD1333 | 002-40280 | MIL-L-46225 | - |
| 27 ± 1.0% | ZIRCONIUM | 000-00950 | MIL-Z-399 | -150 |
| 62 ± 1.0% | LEAD PEROXIDE | 000-15410 | MIL-L-376B | -100 |

NOTES:

1. SIEVES PER RR-S-366 TP 1 CL 1.
2. HANDLE, DRY AND BLEND ALL INGREDIENTS PER MI 002-36290.

NAVAIR DWG. 488AS155

| | | | | | | | |
|--|------|------|----------|--|--|--|--|
| | | | | PRIMER OUTPUT MIXTURE | | | |
| | | | |  ATLAS CHEMICAL INDUSTRIES, INC. WILMINGTON 99, DEL. AEROSPACE COMPONENTS DIVISION | | | |
| SCALE DRAWN BY JDH CHECKER PROJECT ENG. RDW APPROVED BY RDW APPROVED BY <i>RDW</i> DATE 6-16-75 | | | | SHEET 1 OF 1 NO. 002-36290 | | | |
| MAT'L: UNLESS OTHERWISE NOTED DIMENSIONS ARE IN INCHES FRACTIONS ± ANGLES ± DECIMALS ± FINISH IS IN MICROINCHES | | | | NEXT ASST. REVISIONS | | | |
| REV. | ENCL | DATE | APPROVED | | | | |

PRIMING INPUT MIX


NOTE 2


| COMPOSITION BY WEIGHT | MATERIAL | ICI-PN | SPECIFICATION | SIEVE SIZE NOTE 1 |
|--------------------------|----------------------|-----------|------------------------|----------------------|
| 40 ± 2.0% | BASIC LEAD STYPHNATE | 002-40151 | MIL-L-16355(WP) | |
| 5 ± 0.5% | TETRACENE | 002-40161 | MIL-T-46938(MU) | THRU 325 |
| 15 ± 1.5% | ANTIMONY TRISULFIDE | 000-15780 | MIL-A-159 CLASS 2 OR 5 | -140 + 200 |
| 20 ± 2.0% | BARIUM NITRATE | 000-15800 | MIL-B-162 CLASS 1 OR 3 | -70 + 140 |
| 20 ± 2.0% | LEAD AZIDE, RD1333 | 002-40280 | MIL-L-46225 | |

NOTES:

1. SIEVES PER RR-S-366 TP 1 CL 1.
2. HANDLE, DRY AND BLEND ALL INGREDIENTS PER MI 002-40112

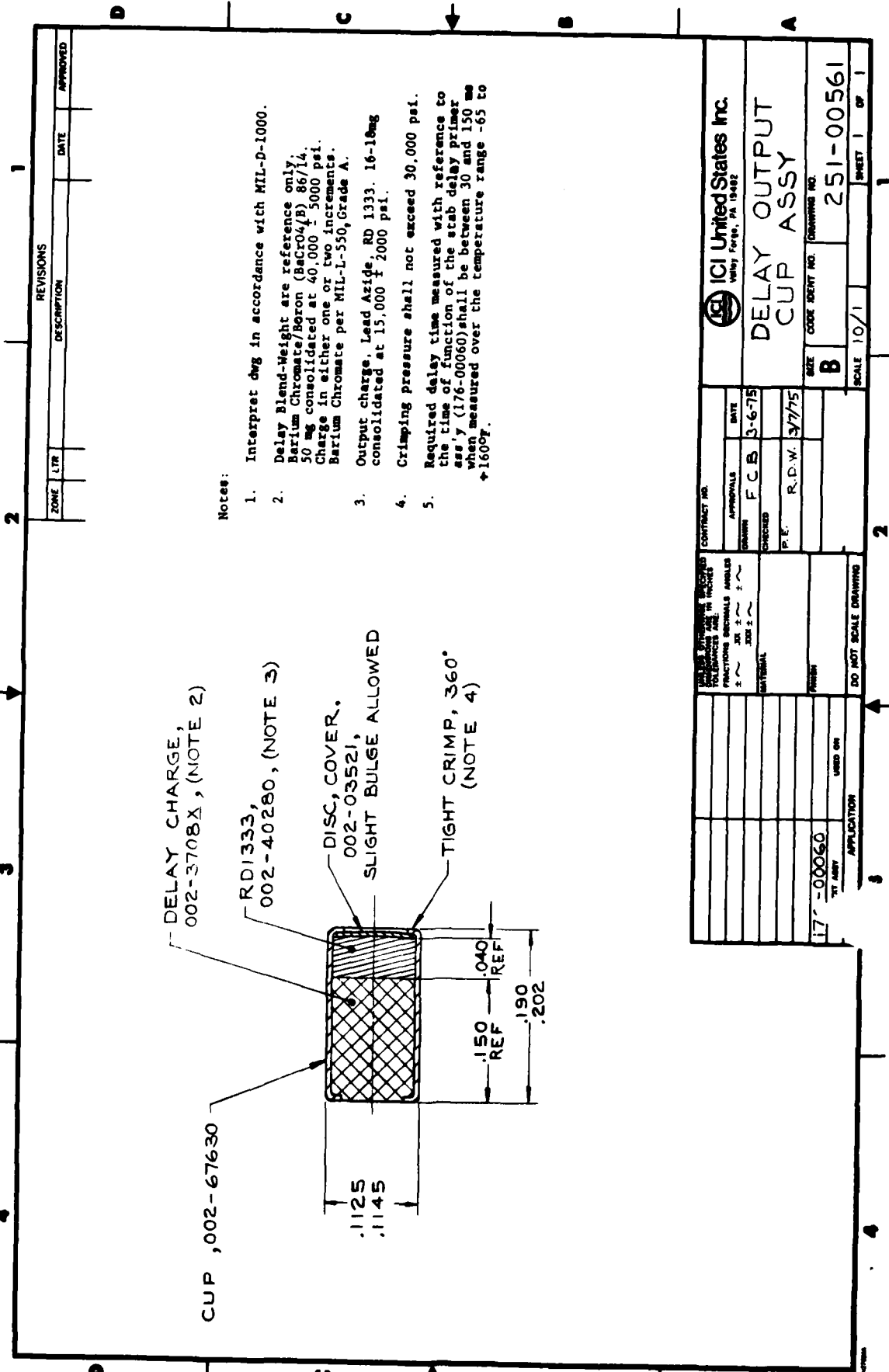
NAVAIR DWG 488AS155


| | | | |
|--|---------------|---|-------------------|
| PRIMING INPUT MIX | | | |
|  ATLAS CHEMICAL INDUSTRIES, INC. WILMINGTON 99, DEL. AEROSPACE COMPONENTS DIVISION | | | |
| SCALE | DRAWN BY: JDH | CHECKER | PROJECT ENG: RDW |
| | | | APPROVED BY: RDW |
| | | | APPROVED BY: JG/3 |
| | | | DATE: 6-16-75 |
| | | NEXT ASST. | |
| MATERIAL: | | UNLESS OTHERWISE NOTED DIMENSIONS ARE IN INCHES FRACTIONS ± ANGLES ± DECIMALS ± FINISH IS IN MICRONS | |
| REV. | QCL | DATE | APPROVED |
| REVISIONS | | | |
| SHEET 1 OF 1 | | NO. 002-40112 | |

| APPLICATION | | | REVISION | | | | | | | | | | | | |
|---|----------------|--|-------------|--|----------|------------------|----------------|--------------------------|---------|--|--|--|--|---|--|
| NEXT ASSY | USED ON | LTR | DESCRIPTION | DATE | APPROVED | | | | | | | | | | |
| <p>PROCESSED LEAD AZIDE RD1333</p> <p>per M.I. 002-40280</p> <p>RAW MATERIAL IS LEAD AZIDE RD1333</p> <p>per MIL-L-46225</p> <p>(000-15950)</p> | | | | | | | | | | | | | | | |
| <small>UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE:</small> <small>FRACTIONS DECIMALS ANGLES</small> ± .XX ± ± ± .XXX ± | | <small>CONTRACT NO.</small> <table border="1"> <tr> <th>APPROVALS</th> <th>DATE</th> </tr> <tr> <td>DRAWN <i>HEP</i></td> <td>12/2/81</td> </tr> <tr> <td>CHECKED <i>JNE</i></td> <td>12/2/81</td> </tr> <tr> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> </tr> </table> | | APPROVALS | DATE | DRAWN <i>HEP</i> | 12/2/81 | CHECKED <i>JNE</i> | 12/2/81 | | | | |  ICI Americas Inc. Valley Forge, PA 19482 | |
| APPROVALS | DATE | | | | | | | | | | | | | | |
| DRAWN <i>HEP</i> | 12/2/81 | | | | | | | | | | | | | | |
| CHECKED <i>JNE</i> | 12/2/81 | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| <small>MATERIAL</small> FINISH | | PROCESSED LEAD AZIDE RD1333 | | <table border="1"> <tr> <td>SIZE A</td> <td>CODE IDENT NO.</td> <td>DRAWING NO. 002-40280</td> </tr> </table> | | SIZE A | CODE IDENT NO. | DRAWING NO. 002-40280 | | | | | | | |
| SIZE A | CODE IDENT NO. | DRAWING NO. 002-40280 | | | | | | | | | | | | | |
| DO NOT SCALE DRAWING | | SCALE | | SHEET 1 OF 1 | | | | | | | | | | | |

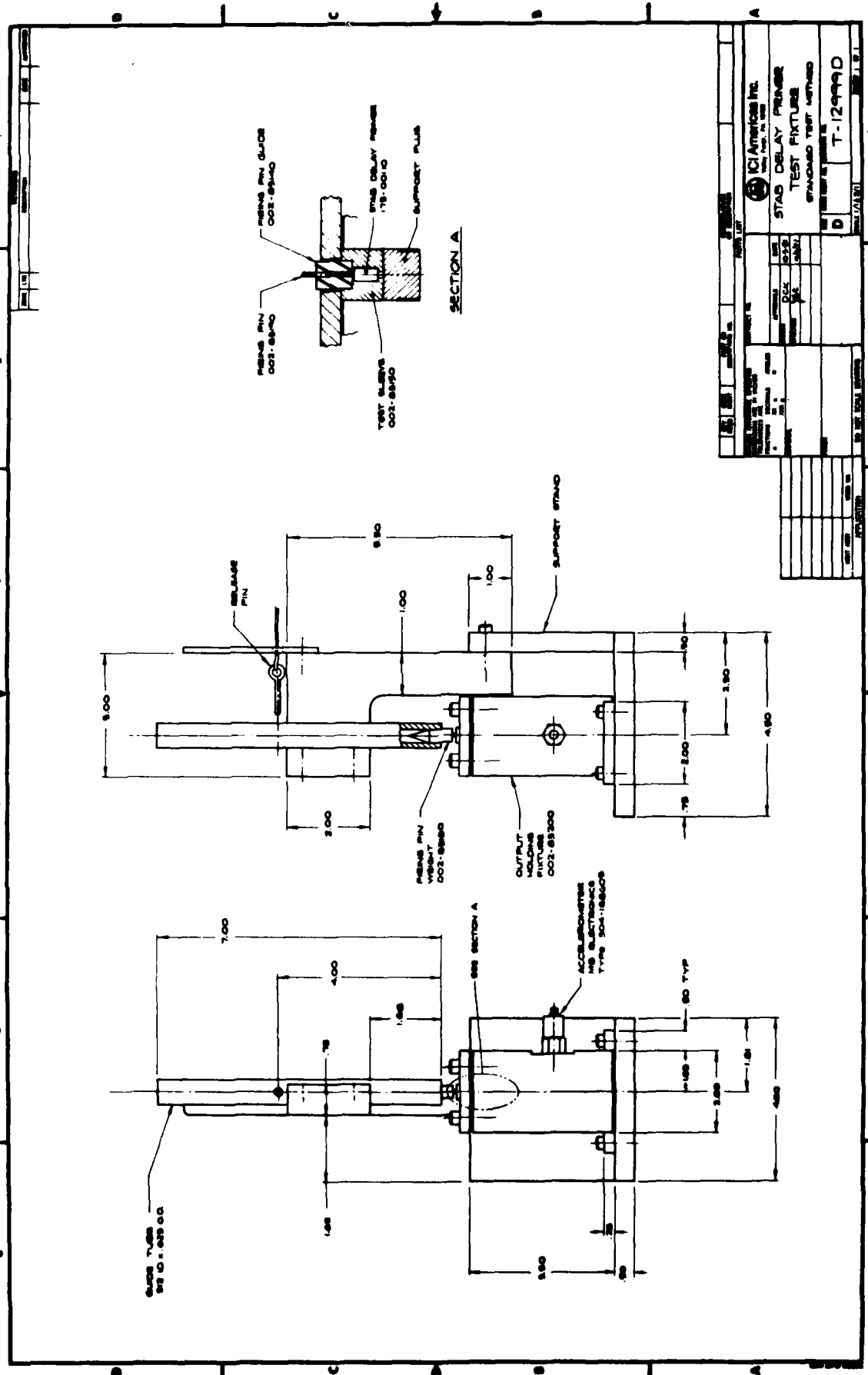
DRAWING 40280 47753

APPENDIX B.--0.1-S STAB DELAY PRIMER DRAWINGS



| | | | |
|--|---|---|--|
|  ICI United States Inc. <small>Wiley, Forge, PA 15402</small> | | DELAY OUTPUT CUP ASSY | |
| CONTRACT NO. APPROVALS DRAWN F C B DATE 3-6-75 CHECKED P.E. R.D.W. 3/7/75 | SIZE B CODE IDENT NO. 251-00561 SCALE 10/1 SHEET 1 OF 1 | 17"-00060 USED ON APPLICATION DO NOT SCALE DRAWING | |

APPENDIX C.--ICI STAB DELAY PRIMER TEST FIXTURE



APPENDIX D.--PREPRODUCTION TEST RESULTS

ICI UNITED STATES INC.
(Atlas Aerospace Division)

H. D. L. Primer

Development Laboratory Report

Date: 2-18-80
Proj # 1369
Sht 1 of 3

Breco Pin .067
Doc # Dfg

| | | Good Guide RD 1333 25.ing | A1A 160-2 11.ing | Empty Spaced to top | | | | Good Guide RD 1333 25.ing | A1A 160-2 11.ing | Empty Spaced to top |
|----|-------------|---------------------------------|------------------------|---------------------------|--|-------------|-------------------|---------------------------------|------------------------|---------------------------|
| | <i>Onus</i> | | | | | <i>Onus</i> | | | | |
| 1 | 12.92 | .103 | .048 | .012 | | 21 | 16.35 | .103 | .048 | .012 |
| 2 | 11.91 | .102 | .048 | .013 | | 22 | 11.86 | .102 | .047 | .013 |
| 3 | 16.13 | .102 | .046 | .015 | | 23 | 16.45 | .100 | .047 | .015 |
| 4 | 15.08 | .103 | .050 | .011 | | 24 | 14.55 | .101 | .046 | .015 |
| 5 | 12.33 | .103 | .047 | .013 | | 25 | 13.16 | .102 | .048 | .012 |
| 6 | 13.73 | .102 | .048 | .012 | | 26 | | | | |
| 7 | 12.01 | .104 | .048 | .011 | | 27 | $\bar{X} =$ 13.33 | | | |
| 8 | 14.08 | .101 | .046 | .016 | | 28 | $S =$ 1.62 | | | |
| 9 | 15.16 | .103 | .048 | .012 | | 29 | | | | |
| 10 | 14.36 | .100 | .047 | .015 | | 30 | | | | |
| 11 | 11.76 | .101 | .047 | .015 | | 31 | | | | |
| 12 | 14.30 | .102 | .048 | .014 | | 32 | | | | |
| 13 | 11.71 | .101 | .046 | .015 | | 33 | | | | |
| 14 | 14.17 | .102 | .048 | .013 | | 34 | | | | |
| 15 | 13.65 | .100 | .048 | .015 | | 35 | | | | |
| 16 | 14.89 | .101 | .047 | .014 | | 36 | | | | |
| 17 | 12.03 | .100 | .046 | .016 | | 37 | | | | |
| 18 | 11.91 | .101 | .045 | .015 | | 38 | | | | |
| 19 | 11.31 | .103 | .047 | .013 | | 39 | | | | |
| 20 | 13.12 | .103 | .047 | .012 | | 40 | | | | |
| | | | | | | | TEST BY: | | | |
| | | | | | | | <i>Test By</i> | <i>Dr. Murphy</i> | | |

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 12.920 | 11.910 | 10.130 | 15.080 | 12.330 |
| 13.730 | 12.010 | 14.080 | 15.160 | 14.360 |
| 11.760 | 14.300 | 11.710 | 14.170 | 13.650 |
| 14.890 | 12.030 | 11.910 | 11.310 | 13.120 |
| 16.350 | 11.860 | 16.450 | 14.550 | 13.160 |

MEAN= 13.317
 SIGMA= 1.620

| | |
|--------|----------|
| 10.130 | X |
| 10.920 | X |
| 11.710 | XXXXXXXX |
| 12.500 | XXX |
| 13.290 | XX |
| 14.080 | XXXXX |
| 14.870 | XXX |
| 15.660 | XX |
| 16.450 | |

F.D. & Primar:

Development Laboratory Report

[illegible]

INPUT DATA

| | | | | |
|-------|--------|--------|--------|-------|
| 9.480 | 11.910 | 12.220 | 11.490 | 8.170 |
| 9.830 | 13.620 | 10.590 | 11.750 | 9.150 |

MEAN= 10.821
 SIGMA= 1.665

| | |
|--------|-----|
| 8.170 | X |
| 8.851 | XX |
| 9.532 | X |
| 10.214 | X |
| 10.895 | X |
| 11.576 | XXX |
| 12.257 | |
| 12.939 | X |
| 13.620 | |

ICI UNITED STATES INC.
(Atlas Aerospace Division)

H.D.L. Primer

Date: 2-25-80

Proj # 1369

Sht 1 of 3

Development Laboratory Report

Baron B. 1067 Force
200# DFG

| | Crow | Lead Bird KD 1333 27.1mg | A1A 160-2 9mg | Space to Top | | | Crow | Lead Bird KD 1333 27.1mg | A1A 160-2 9.1mg | Space to Top |
|----|-------|--------------------------------|---------------------|--------------------|--|----|-------|--------------------------------|-----------------------|--------------------|
| 1 | 9.48 | .107 | .031 | .017 | | 21 | 13.21 | .106 | .040 | .015 |
| 2 | 10.64 | .107 | .039 | .015 | | 22 | 18.26 | .107 | .040 | .014 |
| 3 | 12.94 | .107 | .039 | .015 | | 23 | 14.80 | .107 | .041 | .014 |
| 4 | 12.20 | .108 | .037 | .017 | | 24 | 14.63 | .106 | .040 | .016 |
| 5 | 12.08 | .108 | .039 | .014 | | 25 | 9.86 | .109 | .039 | .015 |
| 6 | 10.58 | .108 | .040 | .013 | | 26 | 12.53 | .109 | .036 | .016 |
| 7 | 9.54 | .108 | .040 | .013 | | 27 | 14.65 | .109 | .038 | .014 |
| 8 | 10.70 | .108 | .039 | .014 | | 28 | 13.22 | .109 | .039 | .014 |
| 9 | 11.29 | .106 | .038 | .017 | | 29 | 11.69 | .109 | .039 | .014 |
| 10 | 10.71 | .107 | .038 | .017 | | 30 | 11.14 | .109 | .040 | .013 |
| 11 | 10.26 | .108 | .038 | .015 | | 31 | 9.62 | .109 | .038 | .014 |
| 12 | 10.23 | .107 | .037 | .016 | | 32 | 12.13 | .109 | .038 | .015 |
| 13 | 9.19 | .108 | .036 | .017 | | 33 | 11.73 | .109 | .039 | .011 |
| 14 | 13.66 | .107 | .040 | .014 | | 34 | 12.87 | .108 | .039 | .014 |
| 15 | 14.77 | .108 | .041 | .012 | | 35 | 13.26 | .109 | .037 | .016 |
| 16 | 11.39 | .109 | .038 | .014 | | 36 | 11.21 | .109 | .038 | .005 |
| 17 | 14.25 | .109 | .038 | .014 | | 37 | 12.66 | .109 | .039 | .014 |
| 18 | 14.33 | .110 | .041 | .012 | | 38 | 10.76 | .110 | .040 | .012 |
| 19 | 12.93 | .108 | .041 | .013 | | 39 | 10.81 | .109 | .038 | .015 |
| 20 | 9.77 | .109 | .040 | .012 | | 40 | 10.74 | .109 | .037 | .015 |
| | | | | | | 4 | 11.99 | test by | | |
| | | | | | | 5 | 1.89 | | | |

SAPLT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 9.480 | 10.640 | 12.940 | 12.200 | 12.080 |
| 10.580 | 9.540 | 10.700 | 11.290 | 10.710 |
| 10.260 | 10.830 | 9.190 | 13.060 | 14.770 |
| 11.390 | 14.250 | 14.330 | 12.930 | 9.770 |
| 13.210 | 18.260 | 14.800 | 14.630 | 9.860 |
| 12.530 | 14.050 | 13.220 | 11.690 | 11.140 |
| 9.620 | 12.130 | 11.730 | 12.870 | 13.260 |
| 11.210 | 12.060 | 10.760 | 10.810 | 10.790 |

MEAN= 11.985
SIGMA= 1.887

| | |
|--------|----------------|
| 9.190 | XXXXXXXX |
| 10.324 | XXXXXXXXXXXXXX |
| 11.457 | XXXXXXXX |
| 12.591 | XXXXXXXX |
| 13.725 | XXXXXX |
| 14.859 | |
| 15.992 | |
| 17.126 | X |
| 18.260 | |

Drying temperature
+150 ° F

ICI UNITED STATES INC.
(Atlas Aerospace Division)

H.D.L. Primer

Date: 2-26-80
Proj # 1369
Sht 2 of 3

Green Line .067
Dome 200*018.

Development Laboratory Report

| | Comp | Seal Gide RD 1333 27-mg | A1A 160-2 9-mg Spec Top | | | Comp | Seal Gide RD 1333 27-mg | A1A 160-2 9-mg Spec Top | |
|----|-------|-------------------------------|-------------------------------------|------|----|-------------------|-------------------------------|-------------------------------------|------|
| 41 | 11.10 | .109 | .041 | .011 | 61 | 11.30 | .109 | .038 | .014 |
| 42 | 9.67 | .108 | .038 | .015 | 62 | 14.29 | .109 | .040 | .012 |
| 43 | 8.75 | .109 | .037 | .015 | 63 | 10.26 | .108 | .037 | .016 |
| 44 | 11.01 | .109 | .037 | .014 | 64 | 13.23 | .109 | .041 | .011 |
| 45 | 12.33 | .110 | .039 | .013 | 65 | 15.61 | .108 | .039 | .013 |
| 46 | 11.24 | .109 | .037 | .015 | 66 | 12.47 | .109 | .040 | .012 |
| 47 | 13.13 | .109 | .042 | .012 | 67 | 11.87 | .108 | .040 | .013 |
| 48 | 16.83 | .109 | .039 | .013 | 68 | 13.51 | .109 | .039 | .013 |
| 49 | 10.61 | .109 | .037 | .015 | 69 | 10.03 | .108 | .035 | .015 |
| 50 | 11.32 | .109 | .041 | .012 | 70 | 11.61 | .109 | .038 | .015 |
| 51 | 9.42 | .110 | .037 | .014 | 71 | 12.35 | .109 | .041 | .012 |
| 52 | 11.56 | .109 | .039 | .014 | 72 | 9.33 | .109 | .041 | .012 |
| 53 | 9.80 | .109 | .041 | .011 | 73 | 10.07 | .110 | .041 | .011 |
| 54 | 11.95 | .109 | .041 | .012 | 74 | 9.58 | .109 | .041 | .011 |
| 55 | 8.38 | .109 | .037 | .014 | 75 | 11.63 | .109 | .038 | .015 |
| 56 | 10.53 | .108 | .037 | .015 | 76 | 10.70 | .110 | .041 | .011 |
| 57 | 11.20 | .110 | .038 | .013 | 77 | 11.15 | .109 | .039 | .014 |
| 58 | 8.46 | .110 | .037 | .015 | 78 | 10.40 | .109 | .038 | .015 |
| 59 | 13.91 | .108 | .041 | .013 | 79 | 11.09 | .108 | .041 | .012 |
| 60 | 10.06 | .109 | .037 | .014 | 80 | 11.42 TEST BY: | .109 | .039 | .014 |
| | | 7 | 11.19 | | 4 | 10.94 | Test By | Sm. Murphy | |
| | | 5 | 1.59 | | 5 | 2.37 | | | |

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 11.100 | 9.670 | 8.750 | 11.010 | 12.330 |
| 11.280 | 13.130 | 10.830 | 10.610 | 11.320 |
| 9.420 | 11.560 | 9.800 | 11.850 | 8.380 |
| 10.530 | 11.200 | 8.400 | 13.910 | 10.060 |
| 11.300 | 14.290 | 10.260 | 13.230 | 15.600 |
| 12.880 | 11.850 | 13.500 | 10.030 | 11.610 |
| 12.350 | 9.330 | 10.070 | 9.580 | 11.630 |
| 10.900 | 11.150 | 10.400 | 11.090 | 11.420 |

MEAN= 11.191
SIGMA= 1.587

| | |
|--------|--------------------|
| 8.380 | XXX |
| 9.282 | XXXXXXXXXX |
| 10.185 | XXXXXXXXXX |
| 11.087 | XXXXXXXXXXXXXXXXXX |
| 11.990 | XXX |
| 12.892 | XXX |
| 13.795 | XX |
| 14.697 | X |
| 15.600 | |

Ambient

ICI UNITED STATES INC.
(Atlas Aerospace Division)

HOL Primer

Date: 2-26-80

Proj # 1369

Sht 3 of 3

Development Laboratory Report

Green Pin .067
Dose 200# DFg

| | | Lead Alloy RD1333 27mg | A1A 160-2 9mg | Spec T ₆ Top | | | | Lead Alloy RD1333 27mg | A1A 160-2 9mg | Spec T ₆ Top |
|-----|-------|------------------------------|---------------------|-------------------------------|-----------|-----------|------|------------------------------|---------------------|-------------------------------|
| | Comp | | | | | Comp | | | | |
| 81 | 11.58 | .105 | .038 | .015 | 101 | 12.45 | .109 | .039 | .013 | |
| 82 | 10.50 | .109 | .035 | .014 | 102 | 12.34 | .110 | .038 | .013 | |
| 83 | 12.41 | .108 | .040 | .013 | 103 | not fired | .109 | .040 | .013 | |
| 84 | 11.05 | .110 | .038 | .014 | 104 | " | .108 | .039 | .014 | |
| 85 | 12.78 | .108 | .038 | .015 | 105 | " | .107 | .040 | .014 | |
| 86 | 9.49 | .108 | .037 | .015 | 106 | " | .108 | .040 | .013 | |
| 87 | 13.65 | .108 | .037 | .015 | 107 | " | .109 | .040 | .012 | |
| 88 | 12.86 | .108 | .034 | .014 | 108 | " | .105 | .039 | .015 | |
| 89 | 9.72 | .108 | .037 | .016 | 109 | " | .108 | .038 | .019 | |
| 90 | 12.41 | .108 | .039 | .014 | 110 | " | .105 | .038 | .015 | |
| 91 | 11.49 | .105 | .038 | .015 | | | | | | |
| 92 | 11.43 | .109 | .041 | .011 | \bar{x} | 11.51 | | | | |
| 93 | 11.22 | .108 | .039 | .014 | S | 11.18 | | | | |
| 94 | 12.04 | .109 | .038 | .014 | | | | | | |
| 95 | 11.79 | .108 | .041 | .013 | | | | | | |
| 96 | 11.86 | .108 | .040 | .014 | | | | | | |
| 97 | 10.62 | .108 | .040 | .012 | | | | | | |
| 98 | 9.01 | .108 | .040 | .014 | | | | | | |
| 99 | 12.28 | .109 | .040 | .012 | | | | | | |
| 100 | 12.01 | .109 | .040 | .012 | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |

TEST BY:

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 11.880 | 10.500 | 12.410 | 11.050 | 12.780 |
| 9.490 | 13.650 | 12.860 | 9.720 | 12.410 |
| 11.490 | 11.430 | 11.220 | 12.040 | 11.790 |
| 11.860 | 10.620 | 9.010 | 12.280 | 12.010 |
| 12.450 | 10.340 | | | |

MEAN= 11.513
SIGMA= 1.175

| | |
|--------|--------|
| 9.010 | |
| 9.590 | XX |
| 10.170 | X |
| 10.750 | XXX |
| 11.330 | XX |
| 11.910 | XXXXX |
| 12.490 | XXXXXX |
| 13.070 | XX |
| 13.650 | X |

APPENDIX E.--FINAL INSPECTION AND TEST PROCEDURE

Prepared By: DNB

Approved By: JTML

Effective Date: 5/20/80



STAB DELAY PRIMER ASSEMBLY

ICI Americas Inc.

Atlas Aerospace Division

Part No.: 176-00110

Operation No.:

Inspection Instruction

Page 1 of 4

| Characteristic Number | Characteristic | Class of Defect | AQL - LPTD | Inspection Device Code | Standard Practice Instruction |
|-----------------------|------------------|-----------------|------------|------------------------|--|
| | FINAL ACCEPTANCE | | | | |
| 001 | Overall Length | | 1.0 | | .300" maximum |
| 002 | Outside dia. | | 1.0 | | .161" maximum |
| 003 | X-ray | | 50/ lot | | X-ray 50 units per lot. One view-dark for powder check units for the following: 1. Input cup 2-increments of powder PIM POM 2. Baffle screen 3. Output assembly 2-increments of powder DELAY RD 1333 If any discrepancies are found, x-ray lot 100% |
| 004 | Visual | | 100% | | All primers shall be visually inspected prior to testing or shipment for the following: a) Cracks, splits or cut through cup b) Explosive on exterior of assembly c) Explosive exposed at either end d) Input end must have evidence of red epoxy (cup end) e) Output end epoxy must be color coded green and flush to just below crimp f) Sealant missing either end g) Input cup must have at least .06 of its end exposed. Epox not allowed within this diameter. h) Input end cup distorted i) Input cup wrinkled or folded j) Crimp output end not 360° k) Crack at crimp l) Evidence of poor workmanship |

ATL 6148

Prepared By: DNB

Approved By: JTML

Effective Date: 5/20/80



STAB DELAY PRIMER ASSEMBLY

ICI Americas Inc.

Atlas Aerospace Division

Part No.: 176-00110

Operation No.:

Inspection Instruction

Page 2 of 4

Characteristic
Number

Characteristic

Class of
Defect

AQL - LPTD

Inspection
Device Code

Standard Practice Instruction

005 Sample

100 primers shall be selected for input energy - delay time - output energy tests.

50 primers shall be selected and sent to HDL for shock tests as specified in characteristics, I.6.1 and I.6.2.

006 Input energy -
Delay time -
Output energy
tests

100

The 100 primers shall be staked into test sleeve 002-83150. 50 assemblies shall be conditioned for a minimum of 2 hours in a chamber stabilized at -65°F.

50 assemblies shall be conditioned for a minimum of 2 hours in a chamber stabilized at +150°F.

Within one minute after removing a primer assembly from its applicable temperature it will be tested per the following scheme. The following parts are required:

Test sleeve - 002-83150
Firing pin guide - 002-83140
Dent block - 002-83170
Holder - 002-83162
Firing pin - 002-83190
Firing pin weight - 002-83180
Holder and stand off sleeve
Accelerometer - Endevco Model 2211 or equivalent
Oscilloscope - Tektronix model 5103N or equivalent.
Fixture - 002-83200
Drop tube -
Primer - M55
Primer Holder - 002-83150
Equipment set up:

- Connect transducer output to channel A of oscilloscope. Also to external trigger.
- Set scope at 5 volts/div.
- Set time for channel A at 2sec/cm.
- Set A trigger to + and external
- Set B mode
 - A dual
 - A single sweep, B SWP
 - B OUT: + SLOPE

ATL 6148

Prepared By: DNB

Approved By: JTML

Effective Date: 5/20/80



ICI Americas Inc.

Atlas Aerospace Division

Part No.: 176-00110

Operation No.:

Inspection Instruction

Page 3 of 4

| Characteristic Number | Characteristic | Class of Defect | AQL - LPTD | Inspection Device Code | Standard Practice Instruction |
|-----------------------|----------------|-----------------|------------|------------------------|---|
| | | | | | <p>Stab Delay Test Procedures as follows:</p> <ol style="list-style-type: none">1. Insert Dent Block 002-83170 into fixture per drawing 002-83200.2. Insert Holder 002-83162 without primer into fixture.3. Insert Primer Holder 002-83150 into fixture. Also firing pin guide 002-83140. Note: Tape opening of empty primer holder.4. Place fixture in "V" Block under drop tube.5. Sight down tube to check alignment of firing pin guide - adjust "V" block as required.6. Insert firing pin, 002-83190, into firing pin guide.7. Measure height from top of firing pin to top of hole, in drop tube, which holds pin supporting the drop weight. Height should be 3 inches max.8. Remove all parts except dent Block (steps 2 thru 6).9. Place some DC-4 into hole of holder and on Dent Block.10. Place primer, M55, into holder with green side up (visible).11. Place holder with primer into fixture with M55 against dent block.12. Insert Primer 176-00110 with input end up (output facing M55 holder).13. Insert firing pin guide, 002-83140 into input end of primer holder. |

ATL 6148

STAB DELAY PRIMER ASSEMBLY

Prepared By: DNB



ICI Americas Inc.

Atlas Aerospace Division

Part No.: 176-00110

Approved By: JTML

Operation No.:

Effective Date: 5/20/80

Inspection Instruction

Page 4 of 4

| Characteristic Number | Characteristic | Class of Defect | AQL - LPTD | Inspection Device Code | Standard Practice Instruction |
|-----------------------|--|-----------------|------------|------------------------|---|
| 007 | Input Energy - Delay Time - Output energy tests on units subjected to shock pulses | 50 | | | <p>14. Place hold down clamp over assembly and tighten the four screws.</p> <p>15. Place fixture against "V" block under drop tube.</p> <p>16. Carefully insert firing pin into firing pin guide.</p> <p>17. Insert weight restraining pin.</p> <p>18. Place weight in drop tube.</p> <p>19. Close firing booth door.</p> <p>20. Reset scope.</p> <p>21. Pull weight restraining pin.</p> <p>22. Remove primer. Reset scope.</p> <p>23. Verify drop tube is clear.</p> <p>24. Repeat steps 9 through 23 for each primer.</p> <p>The 50 primers sent at HDL for shock tests shall be tested after shock tests, per steps 1 thru 24 above (Characteristic Number 006)</p> |

ATL 6148

APPENDIX F.--PILOT LOT TEST RESULTS

LAB. TEST REPORT



ATLAS AEROSPACE DIVISION

| Dwg/part # 176-00110 | | Part name STAB DELAY PRIMER AB-4 | | Test date 10-2-80 | | | | | |
|---|-------------------|-------------------------------------|--------------|---|----------|-------------------|----------------------|--------|-------------|
| Customer order # DAAK21-74-R-9064 | | Atlas order # 1369 | | Lot # 1369-001 | | | | | |
| Sample size 50 | | Spec. # PER CONTRACT | | Spec. par. F. 2.6 | | | | | |
| High 22.0 | | Low 10.0 | | K 14.43 | | | | | |
| Sigma 2.47 | | No fire | | All fire 1/402 4" | | | | | |
| Environment: FOLLOWING HBL SNACK AMBIENT | | | Environment: | | | | | | |
| # | Ohms | no-fire acc. rel. | DENT | Time (MSEC) | # | Ohms | no-fire acc. rel. | DENT | Time (MSEC) |
| 1 | | ✓ | .014 | 17.0 | 26 | | ✓ | .007 | 12.0 |
| | | ✓ | .016 | 15.0 | | | ✓ | .013 | 16.0 |
| | | ✓ | .012 | 13.0 | | | ✓ | .007 | 11.0 |
| | | ✓ | .015 | 11.5 | | | ✓ | .013 | 17.0 |
| 5 | | ✓ | .013 | 11.0 | 30 | | ✓ | .011 | 18.5 |
| | DID NOT FIRE M-55 | | | | | | ✓ | .012 | 13.0 |
| | | ✓ | .015 | 16.0 | | | ✓ | .018 | 14.5 |
| | | ✓ | .007 | 12.5 | | | ✓ | .009 | 14.5 |
| | | ✓ | .014 | 12.0 | | | ✓ | .008 | 11.0 |
| 10 | | ✓ | .018 | 17.0 | 35 | DID NOT FIRE M-55 | | | |
| | | ✓ | .011 | 12.0 | | | ✓ | .007 | 13.5 |
| | | ✓ | .015 | 17.0 | | | ✓ | .014 | 15.0 |
| | DID NOT FIRE M-55 | | | | | | ✓ | .014 | 20.0 |
| | | ✓ | .013 | 14.0 | | | ✓ | .017 | 13.0 |
| 15 | | ✓ | .015 | 13.5 | 40 | | ✓ | .015 | 13.5 |
| | | ✓ | .016 | 11.5 | | | ✓ | .016 | 22.0 |
| | | ✓ | .014 | 11.0 | | | ✓ | .017 | 17.5 |
| | | ✓ | .011 | 15.5 | | | ✓ | .015 | 12.0 |
| | | ✓ | .011 | 13.5 | | | ✓ | .014 | 10.5 |
| 20 | | ✓ | .010 | 21.0 | 45 | | ✓ | .017 | 13.5 |
| | | ✓ | .015 | 14.5 | | | ✓ | .017 | 10.0 |
| | | ✓ | .012 | 16.0 | | | ✓ | .018 | 13.5 |
| | | ✓ | .010 | 20.5 | | | ✓ | .014 | 15.5 |
| | | ✓ | .017 | 18.0 | | DID NOT FIRE M-55 | | | |
| 25 | | ✓ | .014 | 13.0 | 50 | | ✓ | .015 | 11.0 |
| PULL TEST | | BEND TEST | | RESISTANCE | | OUTPUT | | DUDS | |
| Sample | Failures | Sample | Failures | Sample | Failures | Sample | Failures | Sample | Failures |
| | | | | | | 46 | 0 | 50 | 4 |
| MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | Test personnel: <u>Frank Haver</u> | | MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | | | | |
| WITNESSED <u>J. Zambelli</u> DCMS QAR Government Inspector | | | | <u>J. Tadivano</u> Final Inspection Technician | | | | | |

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 17.000 | 15.000 | 13.000 | 11.500 | 11.000 |
| 16.000 | 12.500 | 12.000 | 17.000 | 12.000 |
| 17.000 | 14.000 | 13.500 | 11.500 | 11.000 |
| 15.500 | 13.500 | 21.000 | 14.500 | 16.000 |
| 20.500 | 18.000 | 13.000 | 12.000 | 16.000 |
| 11.000 | 17.000 | 18.500 | 13.000 | 14.500 |
| 14.500 | 11.000 | 13.500 | 15.000 | 20.000 |
| 13.000 | 13.500 | 22.000 | 17.500 | 12.000 |
| 10.500 | 13.500 | 10.000 | 13.500 | 15.500 |
| 11.000 | | | | |

MEAN= 14.435
SIGMA= 2.966

| | |
|--------|--------------|
| 10.000 | XXXXXXXX |
| 11.500 | XXXXXXXX |
| 13.000 | XXXXXXXXXXXX |
| 14.500 | XXXXXXXX |
| 16.000 | XXXXXXXX |
| 17.500 | XXX |
| 19.000 | X |
| 20.500 | XXX |
| 22.000 | |

LAB. TEST REPORT



ATLAS AEROSPACE DIVISION

| | | | | | | | | | |
|---|-------------------|-------------------------------------|--------------|---|----------|-------------------|----------------------|--------|---------------|
| Dwg/part # 176-00110 | | Part name STAB DELTA PRIMER ASSY | | Test date 10-1-80 | | | | | |
| Customer order # DAAK21-79-R-9064 | | Atlas order # 1369 | | Lot # 1369-001 | | | | | |
| Sample size 50 | | Spec. # PER CONTRACT | | Spec. par. F.2.4 | | | | | |
| High 24.0 | | Low 8.5 | | X 15.09 15.16 | | | | | |
| Sigma 3.18 3.19 | | No fire | | All fire 1/4 02 4" | | | | | |
| Environment: -65°F 24 HRS MIN | | | Environment: | | | | | | |
| # | Ohms | no fire acc. rel. | DEPT | Time (M SECS) | # | Ohms | no fire acc. rel. | DEPT | Time (M SECS) |
| 1 | | V | .012 | 12.5 | 26 | | V | .010 | 14.5 |
| | | V | .009 | 13.0 | | | V | .013 | 14.0 |
| | | V | .009 | 8.5 | | DID NOT FIRE M-SS | | | |
| | | V | .011 | 23.0 | | | V | .011 | 15.5 |
| 5 | | V | .012 | 13.0 | 34 | | V | .010 | 17.5 |
| | | V | .011 | 12.0 | | | V | .010 | 13.0 |
| | | V | .013 | 12.5 | | | V | .008 | 15.0 |
| | | V | .014 | 15.0 | | | V | .015 | 21.0 |
| | | V | .008 | 10.5 | | | V | .014 | 14.5 |
| 10 | | V | .011 | 12.0 | 26 | | V | .016 | 14.0 |
| | | V | .013 | 13.0 | | | V | .011 | 13.5 |
| | | V | .012 | 17.0 | | | V | .008 | 19.5 |
| | | V | .011 | 14.0 | | | V | .008 | 12.5 |
| | | V | .012 | 17.0 | | | V | .012 | 18.0 |
| 15 | | V | .008 | 11.0 | 20 | | V | .013 | 13.5 |
| | | V | .009 | 13.0 | | | V | .011 | 24.0 |
| | | V | .010 | 20.0 | | | V | .011 | 17.0 |
| | DID NOT FIRE M-SS | | | | | | V | .011 | 13.5 |
| | | V | .010 | 17.0 | | | V | .011 | 15.0 |
| 20 | | V | .008 | 17.0 | 25 | | V | .009 | 14.5 |
| | | V | .009 | 17.5 | | | V | .011 | 14.0 |
| | | V | .010 | 17.5 | | | V | .012 | 15.0 |
| | | V | .016 | 14.5 | | DID NOT FIRE M-SS | | | |
| | | V | .012 | 11.0 | | | V | .010 | 13.0 |
| 25 | | V | .013 | 10.0 | 50 | | V | .007 | 18.5 |
| PULL TEST | | BEND TEST | | RESISTANCE | | OUTPUT | | DUDS | |
| Sample | Failures | Sample | Failures | Sample | Failures | Sample | Failures | Sample | Failures |
| | | | | | | 47 | 0 | 50 | 3 |
| MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | Test personnel: <u>Leah, Luber</u> | | MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | | | | |
| WITNESSED <u>J. Zierlein</u> DCAS QAR Government Inspector | | | | <u>J. Foderaro</u> Final Inspection Technician | | | | | |

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 12.500 | 13.000 | 8.500 | 23.000 | 13.000 |
| 12.000 | 12.500 | 15.000 | 10.500 | 12.000 |
| 13.000 | 17.000 | 14.000 | 17.000 | 11.000 |
| 13.000 | 20.000 | 17.000 | 17.000 | 17.500 |
| 17.500 | 14.500 | 11.000 | 20.000 | 14.500 |
| 14.000 | 15.500 | 17.500 | 13.000 | 15.000 |
| 21.000 | 14.500 | 14.000 | 13.500 | 19.500 |
| 12.500 | 18.000 | 13.500 | 24.000 | 17.000 |
| 13.500 | 15.000 | 14.500 | 14.000 | 15.000 |
| 15.500 | 13.000 | | | |

MEAN= 15.085
 SIGMA= 3.123

| | |
|--------|----------------------|
| 8.500 | X |
| 10.438 | XXXXX |
| 12.375 | XXXXXXXXXXXXXXXXXXXX |
| 14.313 | XXXXXXXXXXXX |
| 16.250 | XXXXXXXXXXXX |
| 18.188 | XXX |
| 20.125 | X |
| 22.063 | XX |
| 24.000 | |

LAB. TEST REPORT



ATLAS AEROSPACE DIVISION

| | | | | | |
|---|------------|---|--------------|---|-----------------------|
| Dwg/part # 176-00110 | | Part name STAB DELAY PRIMER Assy | | Test date 10-1-80 | |
| Customer order # DAAK21-79-R-9064 | | Atlas order # 1369 | | Lot # 1369-001 | |
| Sample size 50 | | Spec. # PER CONTRACT | | Spec. par. F. 2.5 | |
| Spec. Min: Max: | | Spec. Min: Max: | | Spec. Min: Max: | |
| High 200 | Low 100 | X 14.20 | K | Sigma 202 | No fire |
| | | | | | All fire 1/4 oz 4" |
| Environment: +150F 2HRS MIN | | | Environment: | | |
| # | Ohms | acc. | re | DENT | Time (M SECS) |
| 1 | | ✓ | | .012 | 13.5 |
| | | ✓ | | .012 | 12.4 |
| | | ✓ | | .011 | 13.5 |
| | | ✓ | | .012 | 10.0 |
| 5 | | ✓ | | .012 | 15.3 |
| | | ✓ | | .010 | 12.0 |
| | | ✓ | | .010 | 12.5 |
| | | ✓ | | .010 | 12.5 |
| | | ✓ | | .011 | 12.0 |
| 10 | | ✓ | | .013 | 12.5 |
| | | ✓ | | .014 | 11.5 |
| | | ✓ | | .010 | 16.0 |
| | | ✓ | | .015 | 14.0 |
| | | ✓ | | .008 | 10.0 |
| 15 | | ✓ | | .008 | 16.5 |
| | | ✓ | | .011 | 16.0 |
| | | ✓ | | .006 | 13.0 |
| DID NOT FIRE M-55 | | | | | |
| | | ✓ | | .008 | 15.0 |
| 20 | | ✓ | | .008 | 13.0 |
| | | ✓ | | .013 | 12.0 |
| | | ✓ | | .012 | 12.5 |
| | | ✓ | | .013 | 12.5 |
| | | ✓ | | .015 | 14.5 |
| 25 | | ✓ | | .010 | 13.0 |
| | | | | | |
| PULL TEST | | BEND TEST | | RESISTANCE | |
| Sample | Failures | Sample | Failures | Sample | Failures |
| | | | | 48 | 0 |
| MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | | MEETS SPEC: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> | |
| WITNESSED J. Zwickler OAS QAR Government Inspector | | Test personnel: L. H. Huber | | J. F. Fuleran Final Inspection Technician | |

INPUT DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 13.500 | 12.400 | 13.500 | 10.000 | 15.300 |
| 12.000 | 12.500 | 12.500 | 12.000 | 12.500 |
| 11.500 | 16.000 | 14.000 | 10.000 | 16.500 |
| 16.000 | 13.000 | 15.000 | 13.000 | 12.000 |
| 12.500 | 12.500 | 14.500 | 13.000 | 18.500 |
| 10.000 | 18.500 | 17.000 | 20.000 | 16.000 |
| 17.000 | 19.000 | 14.000 | 11.000 | 12.000 |
| 18.000 | 17.500 | 11.500 | 16.500 | 15.000 |
| 14.500 | 15.500 | 12.500 | 14.500 | 17.000 |
| 18.000 | 12.000 | 10.500 | | |

MEAN= 14.202
SIGMA= 2.623

| | |
|--------|--------------|
| 10.000 | |
| 11.250 | XXXXX |
| 12.500 | XXXXXXXXX |
| 13.750 | XXXXXXXXXXXX |
| 15.000 | XXXXXX |
| 16.250 | XXXXXXXXX |
| 17.500 | XXXXXX |
| 18.750 | XXXXXX |
| 20.000 | XX |

APPENDIX G.--SURVEY TEST RESULTS

Unbranded
input Cup
Regular Prim-Pom

ess Pin .067
Dorce 200 #DFg.

received upon 1780
ICI UNITED STATES INC.
(Atlas Aerospace Division)

N.D.L. Stab.
Delay Primer

Development Laboratory Report

Date: 1-7-81 & 1-8-81
Proj # RA-1369
Sht 1 of 2

Random Samples taken

| # | Oms | Lead/Like RD1333 28mg | A1A 160-2 8mg | Spec to top | # | Oms | Lead/Like RD1333 28mg | A1A 160-2 8mg | Spec to top |
|----|-------|--|---------------------|-------------------|----|-------|-----------------------------|---------------------|-------------------|
| 1 | 13.94 | | | | 21 | 10.54 | | | |
| 2 | 11.66 | .109 | .032 | .012 | 22 | 10.08 | .109 | .032 | .012 |
| 3 | 10.88 | to | .038 | to | 23 | 10.92 | .115 | .038 | to |
| 4 | 13.82 | .115 | | | 24 | 11.68 | | | .019 |
| 5 | 14.26 | | | .019 | 25 | 11.34 | | | |
| 6 | 14.04 | | | | 26 | 12.24 | | | |
| 7 | 8.44 | delay primer are from build of 500 tested with V.F. fixture | | | 27 | 13.64 | | | |
| 8 | 10.94 | | | | 28 | 12.74 | | | |
| 9 | 11.22 | | | | 29 | 13.12 | | | |
| 10 | 13.92 | | | | 30 | 15.28 | | | |
| 11 | 14.18 | | | | 31 | 12.42 | | | |
| 12 | 10.88 | | | | 32 | 11.84 | | | |
| 13 | 12.58 | | | | 33 | 15.52 | | | |
| 14 | 15.16 | | | | 34 | 12.08 | | | |
| 15 | 12.34 | | | | 35 | 12.32 | | | |
| 16 | 9.84 | | | | | | | | |
| 17 | 11.66 | | | | | | | | |
| 18 | 11.70 | | | | | | | | |
| 19 | 10.42 | | | | | | | | |
| 20 | 10.32 | | | | | | | | |

Continued

TEST BY:

M. Murphy

Ambient
Input Cup
Regular Pin Pom

Mass Pin .067
Once 200# DFg.

ICI UNITED STATES INC.
(Atlas Aerospace Division)

H. D. L. Stahl

Delay Primer

Development Laboratory Report

Random Samples taken

Date: 1-8-81
Proj # P.A. 1369
Sht 2 of 2

Proj # PA 1369

ShL 2 of 2

[illegible]

WFLY DATA

| | | | | |
|--------|--------|--------|--------|--------|
| 13.940 | 11.660 | 10.880 | 13.820 | 14.260 |
| 14.040 | 8.440 | 10.940 | 11.220 | 13.520 |
| 14.180 | 10.880 | 12.580 | 15.160 | 12.340 |
| 8.840 | 11.660 | 11.700 | 10.420 | 10.320 |
| 10.540 | 10.080 | 10.920 | 11.680 | 11.340 |
| 12.240 | 13.640 | 12.740 | 13.120 | 15.280 |
| 12.420 | 11.840 | 15.520 | 12.080 | 12.320 |
| 13.380 | 11.640 | 11.660 | 14.080 | 11.220 |
| 13.460 | 11.920 | 13.160 | 9.960 | 12.320 |
| 13.680 | 17.100 | 11.260 | 13.680 | 14.420 |

MEAN= 12.398
SIGMA= 1.740

| | |
|--------|---------------|
| 8.440 | XX |
| 9.523 | XXXXX |
| 10.605 | XXXXXXXXXXXXX |
| 11.688 | XXXXXXXXXXXXX |
| 12.770 | XXXXXXXXX |
| 13.853 | XXXXXXXXX |
| 14.935 | XXX |
| 16.018 | X |
| 17.100 | |

Input Imp Reg Perm Perm

ATL UNITED STATES, INC.
(Atlas Aerospace Division)

H-D-L Stab.
Delays Primer)

Development Laboratory Report

Date: 1-8-81
Proj # P.A. 1369
Sht 1 of 1

metal firing ^{gun} guide holdowns
plastic " " "

[illegible]

INPUT DATA

| | | | | |
|--------|--------|-------|--------|--------|
| 10.340 | 10.960 | 9.240 | 10.140 | 10.560 |
| 11.240 | 11.460 | 8.540 | 11.140 | 8.920 |

MEAN= 10.254
SIGMA= 1.031

| | |
|--------|-----|
| 8.540 | |
| 8.905 | X |
| 9.270 | XX |
| 9.635 | |
| 10.000 | |
| 10.365 | XX |
| 10.730 | X |
| 11.095 | X |
| 11.460 | XXX |

Amirance

2 part Cup Reg Lin Poms

THE UNITED STATES INC.
(Atlas Aerospace Division)

HDL Stab
Delay Primer
Development Laboratory Report

Date: 1-9-81

Proj # RA-1369

Shc 1 of 1

.067 Press Pin 200# DEF

| .067 Press 1m 200 DEG | | | | | | | | | |
|---|-------|-------------------------------|---------------------|---------------------|---------------------------|-------|-------------------------------|---------------------|---------------------|
| # | Oms | Lead Guide RD 1333 28mg | A1A 160-2 8mg | Space to top | # | Oms | Lead Guide RD 1333 28mg | A1A 160-2 8mg | Space to top |
| | | $\frac{.109}{.115}$ | $\frac{.032}{.038}$ | $\frac{.012}{.019}$ | | | $\frac{.109}{.115}$ | $\frac{.032}{.038}$ | $\frac{.012}{.019}$ |
| new all metal firing pin guide no (teflon) guide | | | | | plastic teflon guide only | | | | |
| 1 | 7.70 | | | | 6 | 15.08 | | | |
| 2 | 6.96 | | | | 7 | 11.06 | | | |
| 3 | 7.80 | | | | 8 | 9.48 | | | |
| 4 | 10.34 | | | | 9 | 14.22 | | | |
| 5 | 9.44 | | | | 10 | 11.72 | | | |
| The drop fixture was changed to ensure that the drop weight would exit from the guide tube prior to hitting the firing pin. | | | | | | | | | |
| TEST BY: M. Murphy | | | | | | | | | |

INPUT DATA

7.700

6.960

7.800

10.340

9.440

MEAN=

8.448

SIGMA=

1.353

6.960

X

7.382

XX

7.805

8.227

8.650

9.072

X

9.495

9.917

X

10.340

INPUT DATA

15.080

11.060

9.480

14.220

11.720

MEAN=
SIGMA=

12.312
2.304

9.480

X

10.180

10.880

X

11.580

X

12.280

12.980

13.680

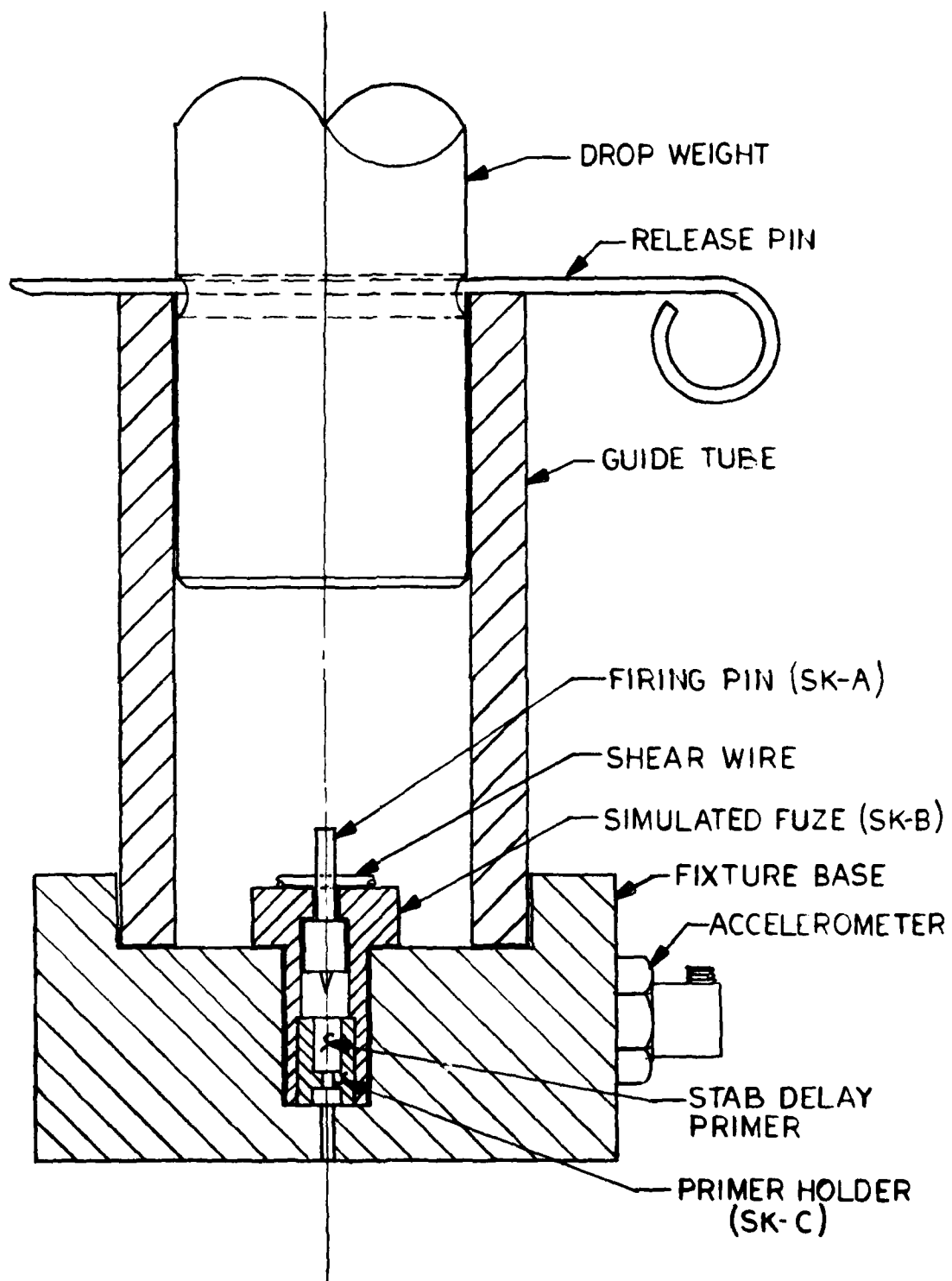
X

14.380

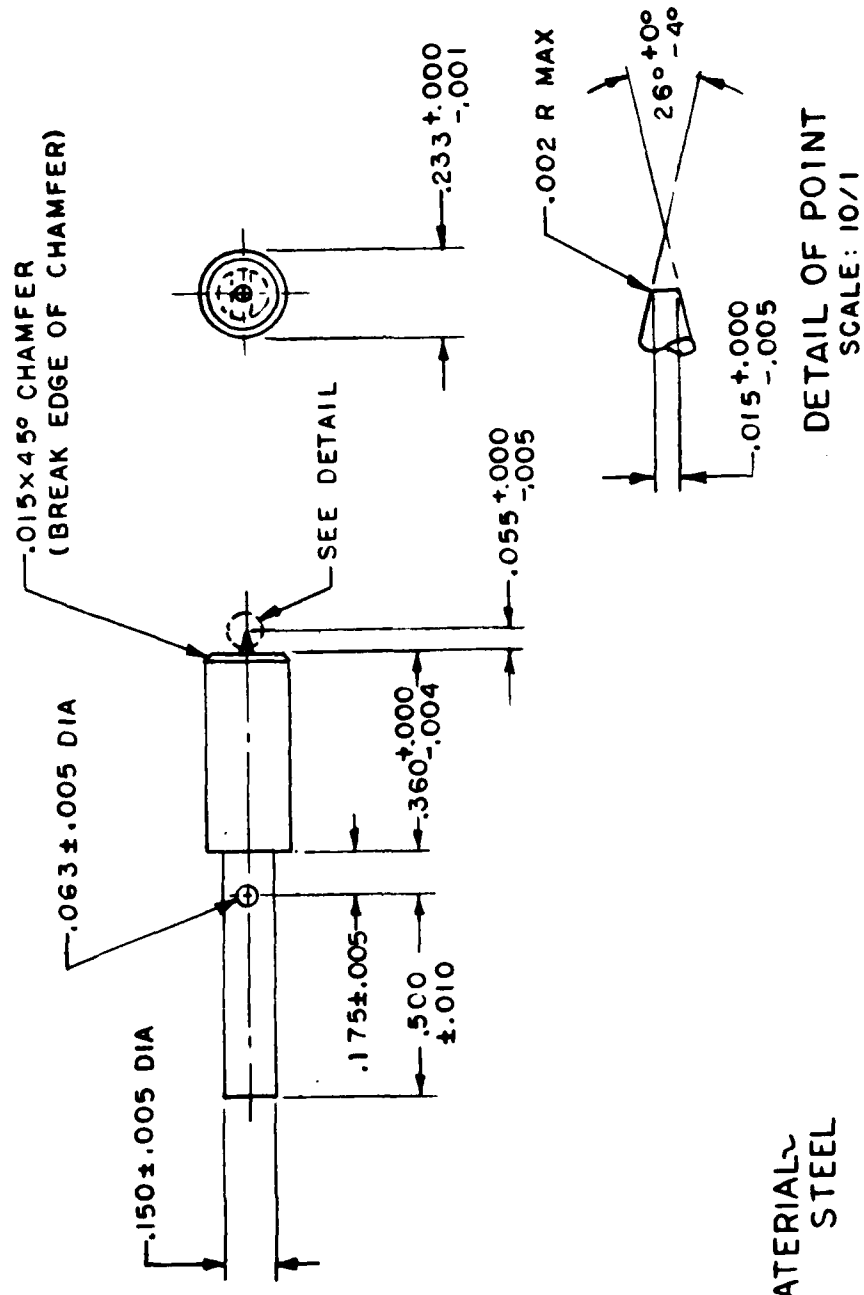
X

15.080

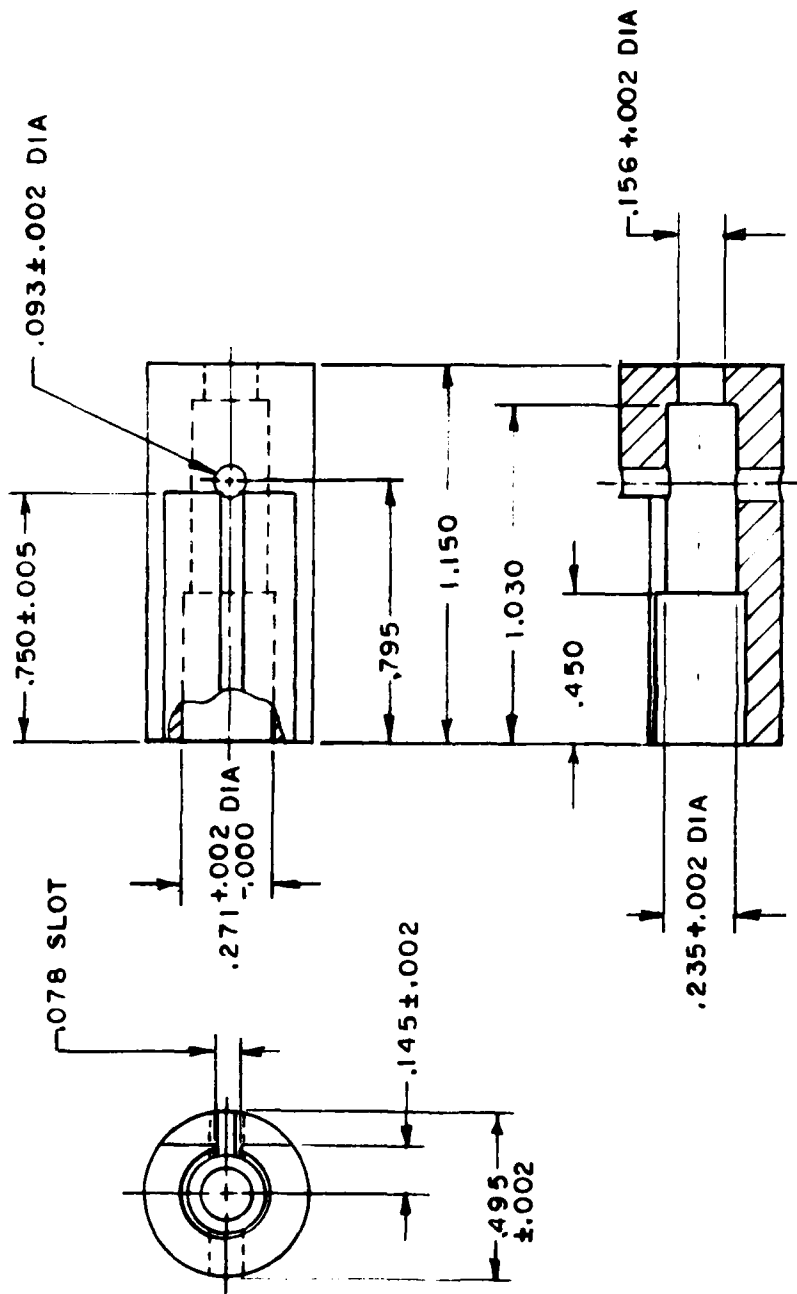
APPENDIX H.--HDL SIMULATED FUZE PRIMER TEST FIXTURE



HDL SIMULATED FUZE PRIMER TEST FIXTURE



FIRING PIN (SK-A)



NOTES:

1. DIM $\pm .005$ IF NOT MARKED.
2. MAT'L ALUMINUM

SIMULATED FUZE (SK-B)



PRIMER HOLDER (SK-C)

NOTES:

1. MIL-A-2550 APPLIES.
2. MATERIAL: ALUMINUM ALLOYS 2011-T3, 2014-T4, 2024, OR 6061-T4 PER ASTM B211.
3. APPLY FINAL PROTECTIVE FINISH NO. 7.3.1 OF MIL-STD-171.

APPENDIX I.--ICI FIXTURE--SPECIAL TEST METHODS

APPENDIX J.--CONFINEMENT TEST RESULTS

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Simulated Fuse Test Fixture +160°F

| TEST NO. | FUNCTION TIME M-SEC |
|----------|---------------------|
| 1 | 8.24 |
| 2 | 8.00 |
| 3 | 8.13 |
| 4 | 9.59 |
| 5 | 7.33 |
| 6 | 8.65 |
| 7 | INPUT 000 |
| 8 | 7.35 |
| 9 | 12.17 |
| 10 | 11.32 |
| 11 | 8.24 |
| 12 | 8.41 |
| 13 | 11.68 |
| 14 | 11.14 |
| 15 | 8.91 |

Test by: Brandi / Murphy

14. INPUT DATA

| | | | | |
|-------|--------|--------|--------|-------|
| 8.240 | 8.000 | 8.130 | 9.590 | 7.330 |
| 8.650 | 7.350 | 12.170 | 11.520 | 8.240 |
| 8.410 | 11.680 | 11.140 | 8.910 | |

MEAN= 9.226
SIGMA= 1.650

7.330

XX

7.733

XX

8.137

XXX

8.540

XX

8.943

9.347

X

9.750

10.153

10.557

10.960

XX

11.363

X

11.767

X

12.170

14. INPUT DATA

| | | | | |
|-------------------|------------------|------------------|------------------|------------------|
| 8.750 | 9.240 | 10.550 | 9.350 | 10.350 |
| 12.100 | 9.200 | 9.000 | 8.700 | 9.300 |
| 9.200 | 8.900 | 10.400 | 9.000 | 10.750 |

MEAN= 9.706
 SIGMA= 0.946

| | |
|-------------------|------|
| 8.700 | XXX |
| 8.983 | XXXX |
| 9.267 | XX |
| 9.550 | X |
| 9.833 | |
| 10.117 | X |
| 10.400 | XX |
| 10.683 | X |
| 10.967 | |
| 11.250 | |
| 11.533 | |
| 11.817 | X |
| 12.100 | |

TRACEBACK FOLLOWS ROUTINE ISN XR1 XR2 ARR
 STAT

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5. Simulated Fuze Test Fixture -65°F

| TEST NO. | FUNCTION TIME M-SEC |
|----------|---------------------|
| 1 | 17.89 |
| 2 | 17.20 |
| 3 | 10.78 |
| 4 | 10.64 |
| 5 | 11.67 |
| 6 | 13.49 |
| 7 | 9.12 |
| 8 | 13.52 |
| 9 | 11.16 |
| 10 | 10.97 |
| 11 | 15.06 |
| 12 | 12.16 |
| 13 | 11.76 |
| 14 | 16.22 |
| 15 | 10.73 |

Test by: Brandi / Evans

| | | | | |
|--------|--------|--------|--------|--------|
| 13.490 | 9.120 | 13.920 | 11.180 | 10.970 |
| 15.060 | 12.160 | 11.760 | 16.220 | 10.730 |

MEAN= 12.825
 SIGMA= 2.652

| | |
|--------|-------|
| 9.120 | X |
| 9.851 | |
| 10.582 | |
| 11.312 | XXXXX |
| 12.043 | XX |
| 12.774 | X |
| 13.505 | X |
| 14.236 | X |
| 14.967 | X |
| 15.697 | X |
| 16.428 | |
| 17.159 | XX |
| 17.890 | |

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CF Test Fixture Maximum Confinement - .020 Penetration +70°F

| TEST NO. | FUNCTION TIME M-SEC | | | | | | |
|-------------|---------------------------|--|--|--|--|--|--|
| 1 | 7.60 | | | | | | |
| 2 | 7.77 | | | | | | |
| 3 | 7.83 | | | | | | |
| 4 | 9.61 | | | | | | |
| 5 | 9.33 | | | | | | |
| 6 | 8.62 | | | | | | |
| 7 | 10.15 | | | | | | |
| 8 | 9.32 | | | | | | |
| 9 | 9.10 | | | | | | |
| 10 | 8.33 | | | | | | |
| 11 | 8.17 | | | | | | |
| 12 | 8.41 | | | | | | |
| 13 | 6.95 | | | | | | |
| 14 | 8.43 | | | | | | |
| 15 | 9.22 | | | | | | |
| 16 | 8.03 | | | | | | |
| 17 | 9.47 | | | | | | |
| 18 | 8.46 | | | | | | |
| 19 | 7.71 | | | | | | |
| 20 | 7.78 | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

Test by: Brandi/Evans

| | | | | |
|-------|--------|-------|-------|-------|
| 7.600 | 7.770 | 7.830 | 9.610 | 9.330 |
| 8.620 | 10.150 | 9.320 | 9.100 | 8.330 |
| 8.170 | 8.410 | 6.950 | 8.430 | 9.220 |
| 8.030 | 9.470 | 8.460 | 7.710 | 7.780 |

MEAN= 8.514
SIGMA= 0.823

| | |
|--------|------|
| 6.950 | |
| 7.217 | X |
| 7.483 | |
| 7.750 | XX |
| 8.017 | XXX |
| 8.283 | XX |
| 8.550 | XXXX |
| 8.817 | X |
| 9.083 | |
| 9.350 | XXXX |
| 9.617 | XX |
| 9.883 | |
| 10.150 | X |

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ICI Test Fixture Minimum Confinement - .020 Penetration +70°F

| TEST NO. | FUNCTION TIME M-SEC | | | | | | | |
|-------------|---------------------------|--|--|--|--|--|--|--|
| 1 | 12.39 | | | | | | | |
| 2 | 12.65 | | | | | | | |
| 3 | 10.40 | | | | | | | |
| 4 | 10.44 | | | | | | | |
| 5 | 10.69 | | | | | | | |
| 6 | 10.84 | | | | | | | |
| 7 | 9.71 | | | | | | | |
| 8 | 10.56 | | | | | | | |
| 9 | 10.26 | | | | | | | |
| 10 | 11.23 | | | | | | | |
| 11 | 10.54 | | | | | | | |
| 12 | 8.56 | | | | | | | |
| 13 | 9.17 | | | | | | | |
| 14 | 8.95 | | | | | | | |
| 15 | 11.01 | | | | | | | |
| 16 | 8.89 | | | | | | | |
| 17 | 8.09 | | | | | | | |
| 18 | 9.34 | | | | | | | |
| 19 | 8.40 | | | | | | | |
| 20 | 9.06 | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |

Test by: Brandi / Murphy

| | | | | |
|-------------------|------------------|-------------------|-------------------|-------------------|
| 12.390 | 12.650 | 10.400 | 10.440 | 10.690 |
| 10.840 | 9.710 | 10.960 | 10.260 | 11.290 |
| 10.540 | 8.560 | 9.170 | 8.950 | 11.010 |
| 8.890 | 8.090 | 9.340 | 8.400 | 9.060 |

MEAN= 10.059
SIGMA= 1.259

| | |
|-------------------|--------|
| 8.090 | |
| 8.470 | XX |
| | X |
| 8.850 | |
| | XXXX |
| 9.230 | |
| | X |
| 9.610 | |
| | X |
| 9.990 | |
| | X |
| 10.370 | |
| | XXXXXX |
| 10.750 | |
| | XX |
| 11.130 | |
| | X |
| 11.510 | |
| 11.890 | |
| 12.270 | |
| | XX |
| 12.650 | |

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1. Test Fixture Maximum Confinement - .060 Penetration +70°F

| TEST NO. | FUNCTION TIME M-SEC |
|----------|---------------------|
| 1 | 10.08 |
| 2 | 8.17 |
| 3 | 7.43 |
| 4 | 9.26 |
| 5 | 7.81 |
| 6 | 6.92 |
| 7 | 9.05 |
| 8 | 8.23 |
| 9 | 10.79 |
| 10 | 8.55 |
| 11 | 9.11 |
| 12 | 9.36 |
| 13 | 10.98 |
| 14 | 13.92 |
| 15 | 8.42 |
| 16 | 7.15 |
| 17 | 9.56 |
| 18 | 10.01 |
| 19 | 8.97 |
| 20 | 8.85 |

Test by: *Brenti / Murphy*

24. INPUT DATA

| | | | | |
|--------|--------|--------|--------|-------|
| 8.290 | 7.380 | 8.220 | 9.050 | 9.800 |
| 9.750 | 8.380 | 10.080 | 10.390 | 8.840 |
| 10.090 | 10.520 | 11.010 | 7.530 | 8.900 |
| 7.780 | 8.930 | 9.360 | 8.160 | 9.930 |

MEAN= 9.116
 SIGMA= 1.049

7.380

XX

7.682

X

7.985

XX

8.287

XX

8.590

X

8.892

XXX

9.195

X

9.497

X

9.800

XXXX

10.102

X

10.405

X

10.707

X

11.010

| | |
|--------------------------------------|----|
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| DEFENSE TECHNICAL INFORMATION CENTER | |
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| ALEXANDRIA, VA 22314 | |
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| SILVER SPRING, MD 20910 | |
| NAVAL SURFACE WEAPONS CENTER | 1 |
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